

The past, present, and future of the molten core method of fiber fabrication

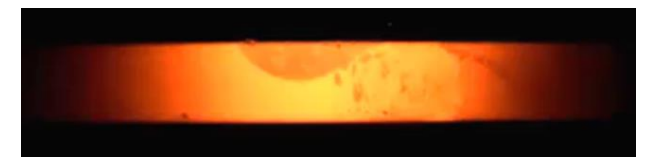
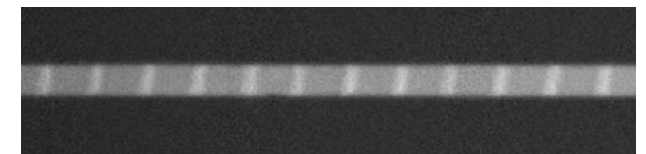
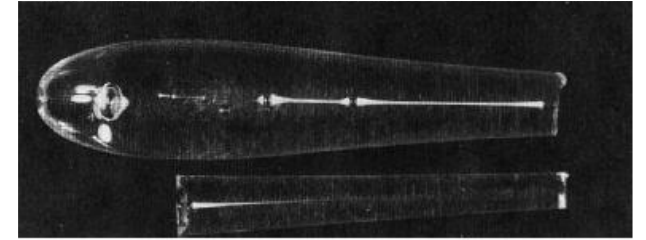
John Ballato

Department of Materials Science and Engineering, Clemson University, Clemson, SC USA

Optica Webinar - Optical Fabrication and Testing (FM) Technical Group

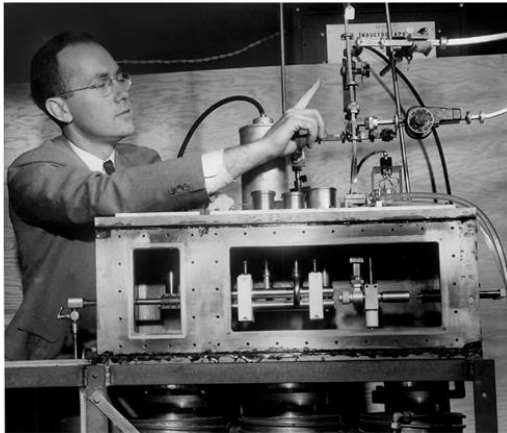
July 2022

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 - Where's here?
 - No. No. No. Maybe. OK. Boom. Whoa.
 - What's next?!?!?

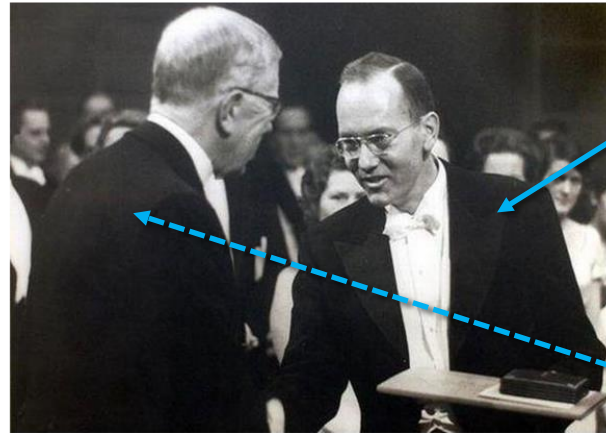


The Past

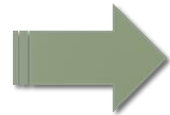
1955: Townes (and Gordon and Zeiger)



10 December 1964: Charles Townes and King Gustaf of Sweden



Father of the laser



1966: Kao (and Hockham)



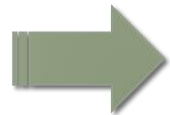
10 December 2009: Charles Kao and King Carl of Sweden



Father of...

Father of optical fiber

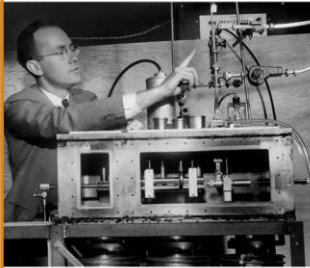
Exactly 45 years later!



The Past

Necessary... but insufficient.

1955: Townes (and Gordon and Zeiger)



10 December 1961: Charles Townes and King Gustaf of Sweden



1966: Kao (and Hockham)



10 December 2009: Charles Kao and King Carl of Sweden



Fathers of actual / useable fiber.

1970: Keck, Maurer, and Schultz

Then the attenuation is:

$$\alpha = \frac{10 \log \frac{40}{355}}{29 \text{ meters}} = 17 \text{ dB/km}$$

Whisper!

Must re-examine this to check!

in lunch, signal is holding
the lower. Measured output
to 850,
100 KHz.

$S_{in} = 158$ input in dBm
 $S_{out} = 159$ (less a couple dB)

$S_{in} = 158$
25.1 meters

$$\frac{37.5}{2.2} = 18.2 \text{ dB/km}$$

Upon the 42.1 meter a correct gain $\alpha = 22$; so we
are definitely in good shape on the guide.
Increased short length in index fluid on the output end got
no signal change.

Fiber diameter is 9.2 mil. Mode patterns for it are on
page 17. λ_0 was 0.49 microns giving $2(\lambda_0^2 - m^2)^2 = 0.376$
For comparison the previous 20 dB/km guide had a value of 0.36 with
 $\lambda_0 = 0.47$ microns. The core diameter is 3.7 microns. This is about
a 1.5% TiO₂ doping in the core. The λ value can then be
calculated for 6328:

$$u = \frac{\pi(3.7)}{0.6328} [m_1(1.0225) - m_2(1.0225)]^{1/2} = \frac{\pi(3.7)}{0.6328} [(1.418) - (1.357)]^{1/2}$$

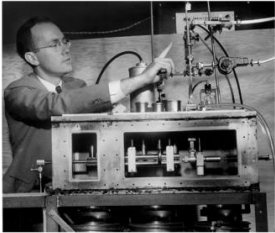
$$= 1.83$$

RESTRICTED
See Protective Order in
Corning v. IIT.

007730

The Past... into... the Present

1955: Townes (and Gordon and Zeiger)



10 December 1964: Charles Townes and King Gustaf of Sweden



1966: Kao (and Hockham)



10 December 2009: Charles Kao and King Carl of Sweden



1970: Keck, Maurer, and Schultz

The structure is:

$$p_0 = 10 \log \frac{1000}{29 \text{ meters}} = 17.44 \text{ dB} \quad \text{Whoops!}$$

Must measure the loss!

my hands, signal is better
by lower. Mechanical signal
is 800.
100 Hz.

Signal = 158 signal in fiber
Signal = 159 (seen a up shift)

Signal = 158
24.1 meters

$$\frac{158}{159} = 18.2 \text{ dB}$$

Using the 24.1 meter = correct gain $p_0 = 22$, so we
are definitely in good shape on the guide.
Increasing short length in order field on the output and not
on signal changes.

Fiber diameter = 9.2 mil. Made pattern for it on
page 17. λ_0 was 0.89 microns giving $d(\lambda_0 - \lambda)^2 = 0.376$
If comparison the pattern to other guide had a value of 0.36 microns
 $\lambda_0 = 0.87 \mu\text{m}$ - the loss should be 3.7 dB. The guide
is 157.5 dB signal in the fiber. The 24 meters on the
calculator for 6.7 dB.

$$d = \frac{\pi (9.2)^2}{0.6328} \left(\frac{1}{m(\lambda_0) - m(\lambda)} \right)^2 = \frac{\pi (9.2)^2 (1.000) - (0.89)^2}{0.6328^2}$$

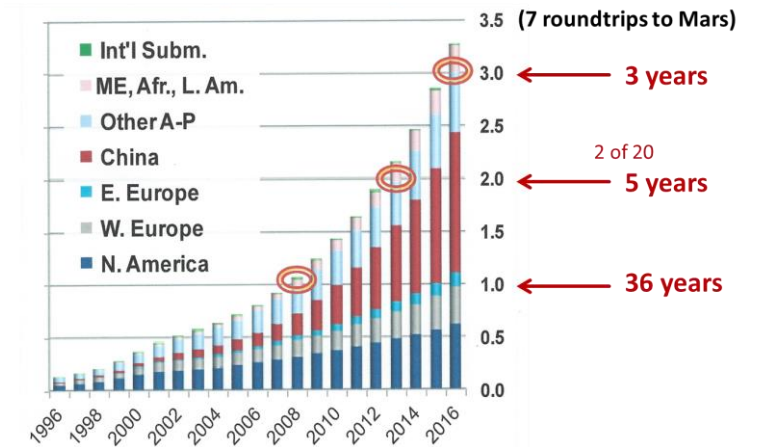
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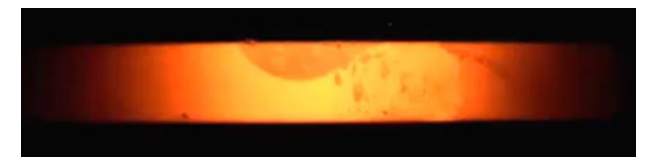
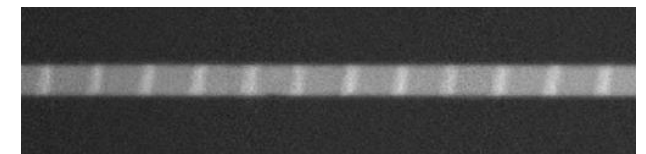
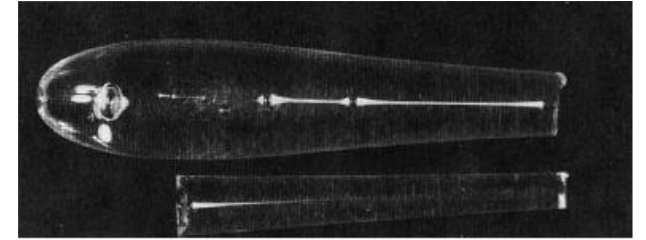
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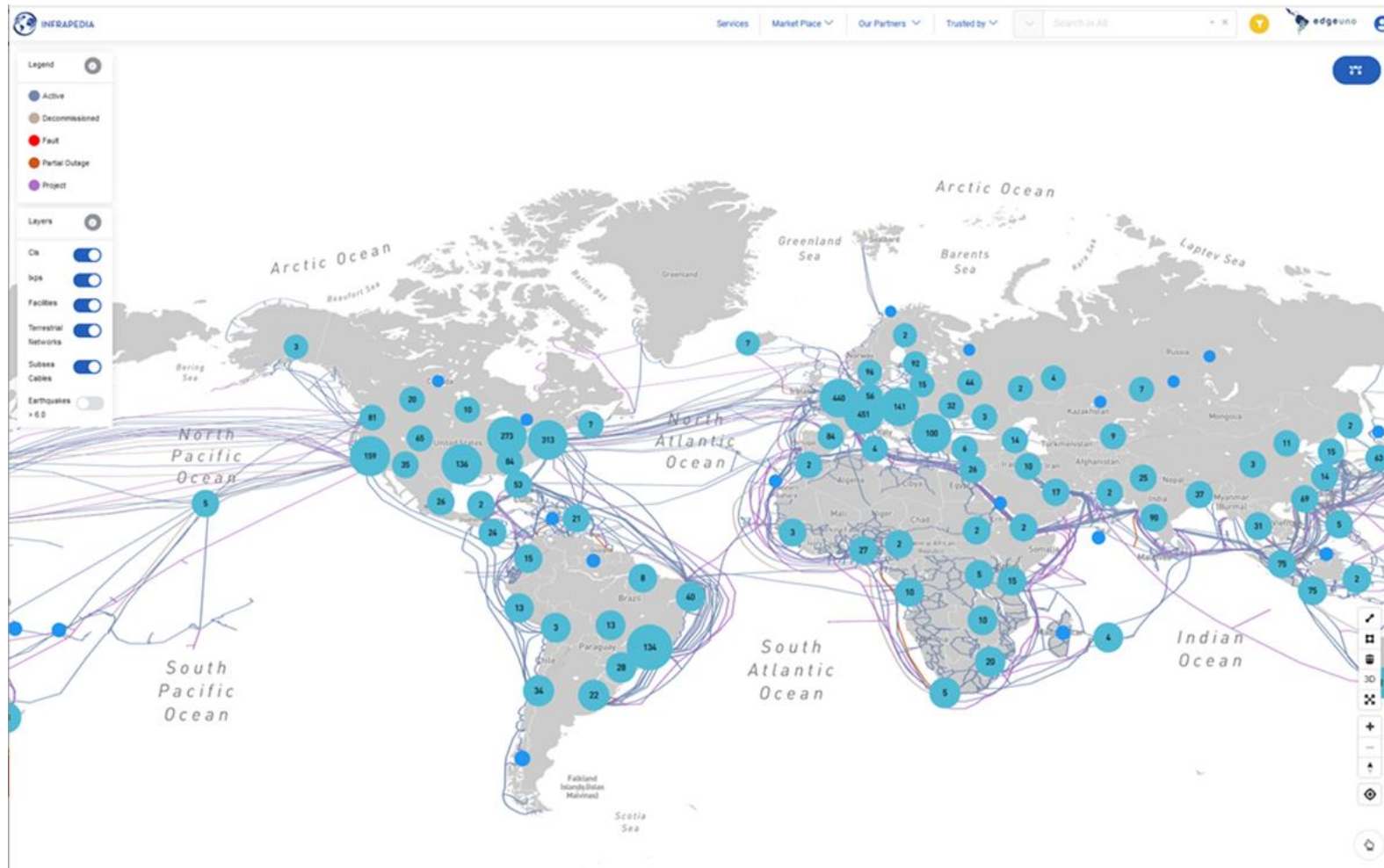
Cumulative total of cabled fiber installed worldwide (billion fiber-km)



-
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The Present



The Present... but...

- Always more... growing demand for ever-more sophisticated fibers and lasers.

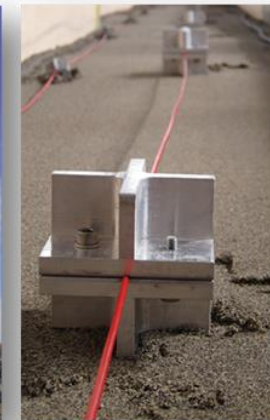
Communications



Machining / Manufacturing



Energy / Sensing / Medicine



Ranging / Science



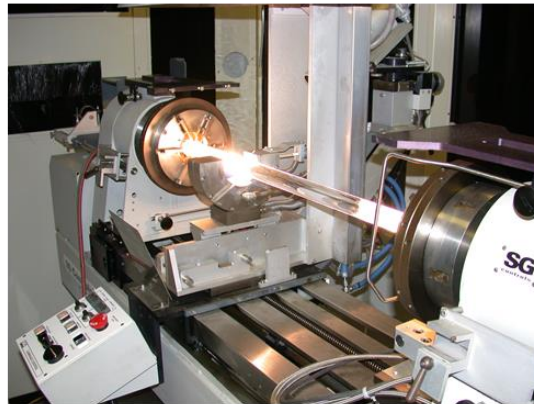
Directed Energy



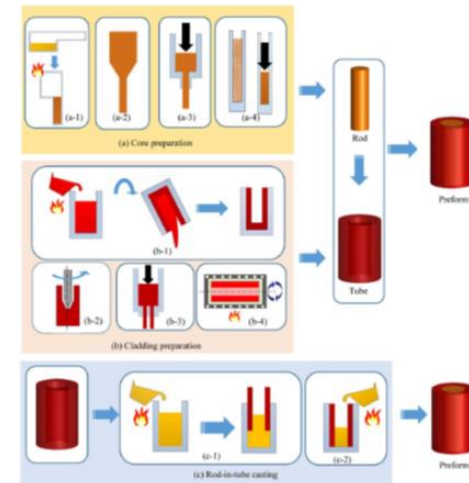
The Present... but...

- Two primary practical methods for making optical fibers.

Form preform via CVD processes (telecom)



Melt and form core and clad glasses (specialty)



- Both require the formation of a (core / clad) preform.
- Both force the glass to go through multiple thermal cycles, thus risking compositional flexibility, due to immiscibilities or glass forming limitations, hence performance limitations.

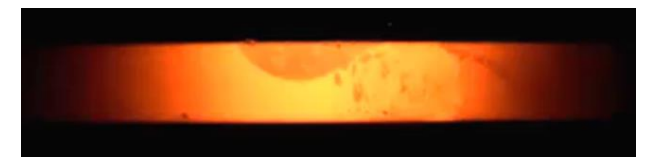
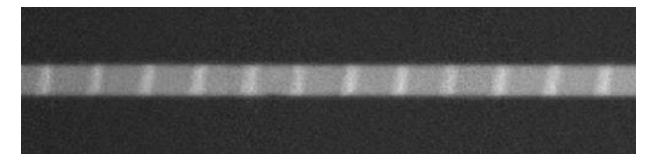
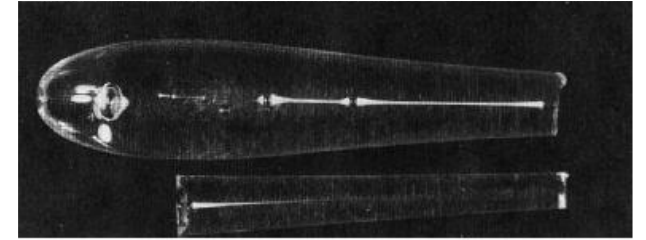
The Present... but...

- Fibers drawn from a preform; either consolidated or as rods / tubes.
- In both cases, compositions are limited by glass-forming ranges, which depend on time and temperature.
- One really needs to pay attention to the underlying materials science to unleash the full potential of the periodic table on fiber properties and performance.

TABLE V. Best effort comparison of maximum (selective) dopant concentrations into silica using selected fiber fabrication methods.

Dopant into SiO ₂	Maximum concentration by fabrication method (mol. %)	
	<i>Vapor deposition</i>	<i>Powder sintering</i>
Al ₂ O ₃	8	8 ⁵⁵⁸
Fluorine	2	2 ⁵⁵⁸
Rare earth oxide	2	6 (Yb ₂ O ₃) ⁵⁵⁸
Alkaline earth oxides	<2 (BaO) ⁴²	
Ta ₂ O ₅	<1 ⁴⁶	
Li ₂ O	0.2 ⁴¹	

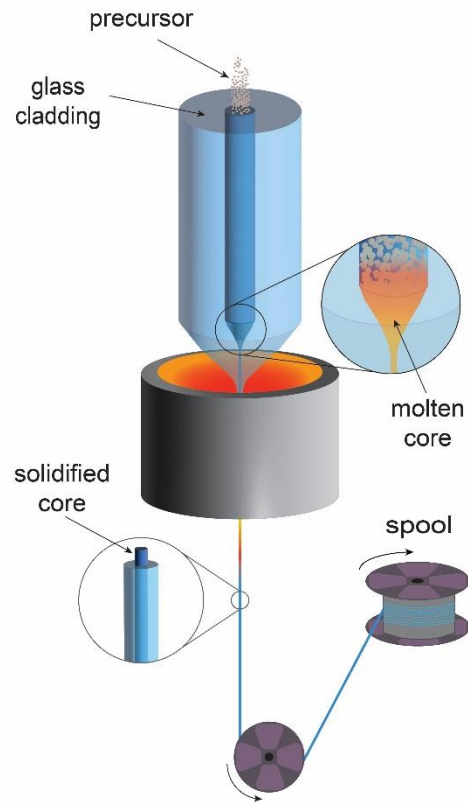
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The molten core method

aka “melt-in-tube,” “powder-in-tube,”
granulated powder,” etc. methods.

- Core phase melts at temperature where cladding glass draws (directly) into fiber.
- Originally... High quench rates permit unstable glasses to be directly fiberized.



Advantages

- Straight-forward
- Industry-accepted manufacturing (fiber draw) used; no lathe deposition.
 - Long lengths (> km)
 - High speed manufacturing (> m/s)
- **Low temperature** (compared to CVD...)
- Can be reactive (liquid-phase chemistry), *we'll get to this...*
- Amendable to very wide range of materials

Disadvantages (?)

- **High temperature** (diffusion/dissolution)
- Non-volatile cores, *we'll get to this...*
- *One must understand materials / glass science*

The Past... again (a quick walk down memory lane...)

Glass Compositions 8/27/92

MC 2522A 69 SiO₂, 15 Na₂O, 10 CaO, 1 Al₂O₃, 3 Na₂CO₃, 2 CeO₂
 primary WO₃ glasses: 3718, 3750, 3780
 #00% Ce (PO₃)₃

#742: 44.69 Tb, 18.68 Al, 36.63 Si

816	"	Ce	"	"
817	"	Pr	"	"
818	22.34 Ce	22.35 Eu	"	"
819	"	Pr	"	"

748 62.6 Si, 12 Na, 3 K, 12.5 Ca, 7.2 Ti, 0.7 Sb, 2.0 Nd
 4.0 Nd

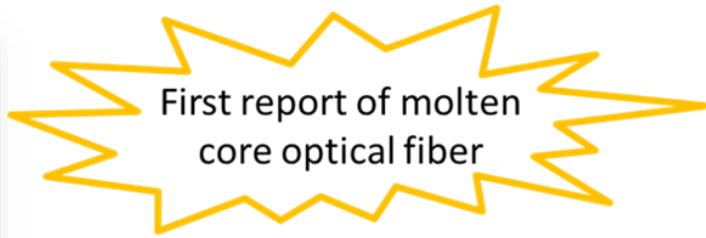
1-2848 26.88 Si, 17.59 Al, 1.10 Sb, 0.5 K, 53.87 La
 1-2849 " " " " " "

2885	28.30 Si	19.40 Al	2.0 Ce	20.6 Y	29.7 La
6			5		26.7
7			10		21.7
8			15		16.7
9			20		11.7
30			31.70		"

2-CR 8 56 La, 4 Mg, 12 Al, 25 Si, 1 Sb, 2 Nd

1-	27 wt% SiO ₂	2-	25 wt% SiO ₂
	18 wt% Al ₂ O ₃		12 " Al ₂ O ₃
	1 wt% Sb ₂ O ₃		1 " Sb ₂ O ₃
	54 wt% Tb ₂ O ₃		4 " MgO
			58 " Tb ₂ O ₃

3- like 2- but
 50 wt% Tb₂O₃
 8 wt% SiO₂ Al



First report of molten core optical fiber

Tuesday Morning, April 20

(Three Concurrent Sessions)

"Optical Materials I: Optical Fiber and Waveguides"

Room: 801

Session Chair: Celia Merzbacher, Naval Research Laboratory, Washington, DC 20375-5338

Break

10:00-10:20 a.m.

10:20-10:40 a.m.

(G-54-98) Rare Earth Doping of Silica Based Fiber by the Sol-Gel Method, F. Wu, E. Snitzer, and G.H. Sigel, Jr., Rutgers University, Piscataway, NJ

10:40-11:00 a.m.

(G-55-98) Fabrication of Fibers with High Rare Earth Concentrations, J. Ballato* and E. Snitzer, Rutgers University, Piscataway, NJ

11:00-11:20 a.m.

(G-56-98) Tellurite Glass Stability for Rare Earth Doping and Fiber Processing, J.S. Wang,* E. Snitzer, and G.H. Sigel, Jr., Rutgers University, Piscataway, NJ; E.M. Vogel, Bellcore, Red Bank, NJ

11:20-11:40 a.m.

(G-57-98) Thermal Stability of Fluoride Glass Optical Fibers, P.J. Melling and L. Vacha, Galileo Electro-Optics Corporation, Sturbridge, MA

11:40 a.m.-12:00 noon

(G-58-98) Thin Film Processing of Al₂O₃ Waveguides, B.H. Stadler* and M. Oliveria, Massachusetts Institute of Technology, Cambridge, MA

Fabrication of fibers with high rare-earth concentrations for Faraday isolator applications

John Ballato and Elias Snitzer

The Faraday effect provides a mechanism for achieving unidirectional light propagation in optical isolators; however, miniaturization requires large Verdet constants. High rare-earth content glasses produce suitably large Verdet values, but intrinsic fabrication problems remain. The novel powder-in-tube method, or a single-draw rod-in-tube method, obviates these difficulties. The powder-in-tube method was used to make silica-clad optical fibers with a high terbium oxide content aluminosilicate core. Core diameters of 2.4 μm were achieved in 125-μm-diameter fibers, with a numerical aperture of 0.35 and a Verdet constant of -20.0 rad/T m at 1.06 μm. This value is greater than 50% for crystals found in current isolator systems. This development could lead to all-fiber isolators of dramatically lower cost and ease of fabrication compared with their crystalline competitors. © 1995 Optical Society of America

1. Introduction

Modern photonic devices for optical computing, telecommunications, etc., require classes of elements that exhibit nonreciprocal behavior. One such class is based on the Faraday effect,¹ in which the rotation of plane-polarized light is dependent on only the applied magnetic field and is not dependent on the direction of light propagation. This provides unidirectional propagation of light in an optical fiber. In this paper we briefly describe this effect to illustrate the factors that influence the Verdet constant,² characterizing the magnitude of the effect, and our choice of the high rare-earth content glass composition for its attainment. This is followed by a short discussion of a novel method of fabricating optical fibers with these constituents and the experimental realization of fibers with large Verdet constants.

2. Faraday Effect

The Faraday effect in glass is a well-understood phenomenon and has been intensively studied and documented.³⁻¹⁰ It is present in all materials and is closely related to the magnetic behavior of the component ions. The rotation varies with temperature in

paramagnetic and ferromagnetic materials, but is temperature independent in diamagnetic materials. Its magnitude also tends to decrease with increasing wavelength. The Faraday effect is a magnetic-field-induced circular birefringence, providing a means of controlling the polarization state of light. The effect is distinct from intrinsic circular birefringence (optical chirality or activity) in that its rotation direction depends on only the direction of the magnetic field along the path of light propagation and not on the direction of light propagation. The optical rotation arises from the inequality of the refractive indices for right- and left-circularly polarized light; these, in turn, stem from the ground- and excited-state splitting in the medium when an external magnetic field is applied.

At a more fundamental level, Faraday rotation can be implicitly inferred from the time-reversal asymmetry of Maxwell's equations. These are

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t},$$

$$\nabla \times \mathbf{H} = \frac{\partial \mathbf{D}}{\partial t} + \mathbf{J},$$

$$\nabla \cdot \mathbf{D} = \rho,$$

$$\nabla \cdot \mathbf{B} = 0.$$

When (t) is replaced with $(-t)$ for \mathbf{E} and \mathbf{D} , this is equivalent to replacing $x, y,$ and z by $(-x), (-y),$ and $(-z),$ respectively [similarly, \mathbf{r} by $(-\mathbf{r})$]. The physical

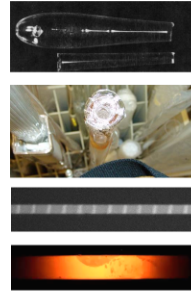
The authors are with the Fiber Optic Materials Research Program, Rutgers, The State University of New Jersey, Piscataway, New Jersey 08855-0909.

Received 21 November 1994; revised manuscript received 31 March 1995.

0003-6935/95/306848-07\$06.00/0.
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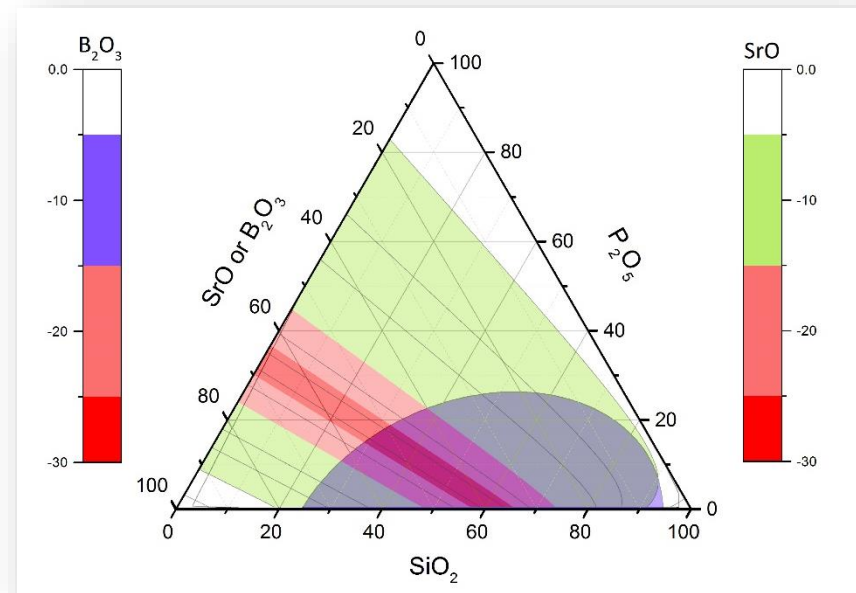
The Past... into... the Present (again)

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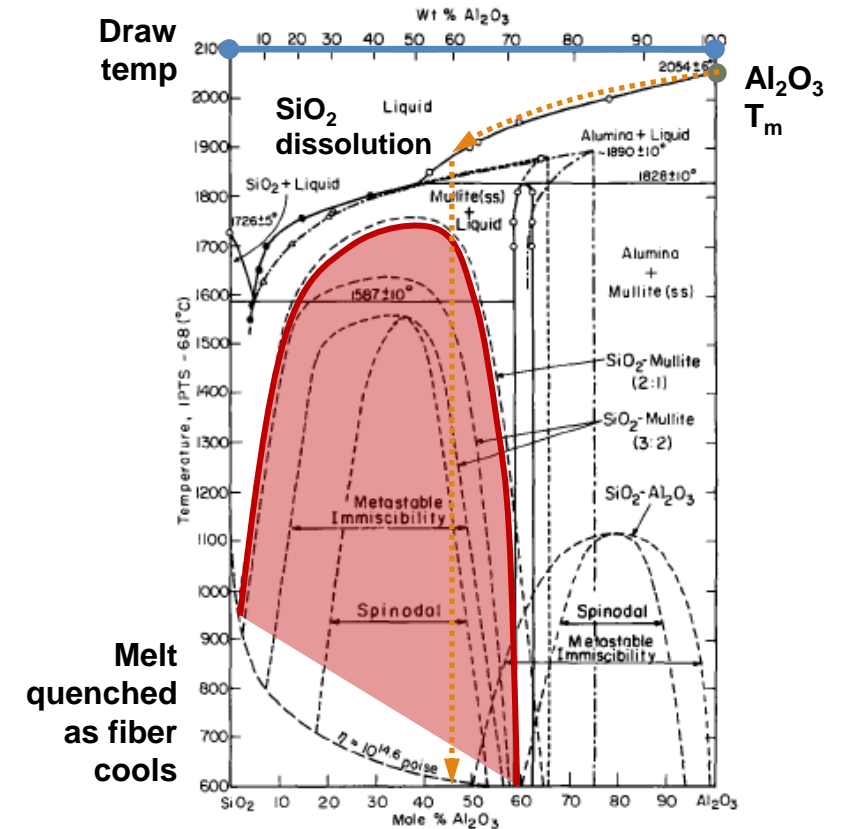
Examples...

1. Intrinsically low nonlinearity all-glass fibers
2. Crystalline semiconductor core fibers



What's new about the $\text{Al}_2\text{O}_3 - \text{SiO}_2$ system?

- The addition of alumina (Al_2O_3) to silica (SiO_2) glass is known to raise the refractive index and to “solubilize” active dopants into the glass.
- However, the doping of alumina in silica is limited for two reasons:
 1. CVD not as amenable to the addition of alumina as they are other dopants (e.g., vapor-phase GeO_2).
 2. Limitation in amount of alumina (~ 10 wt. %) that can be added into silica prior to phase-separation.



What's new about the $\text{Al}_2\text{O}_3 - \text{SiO}_2$ system?

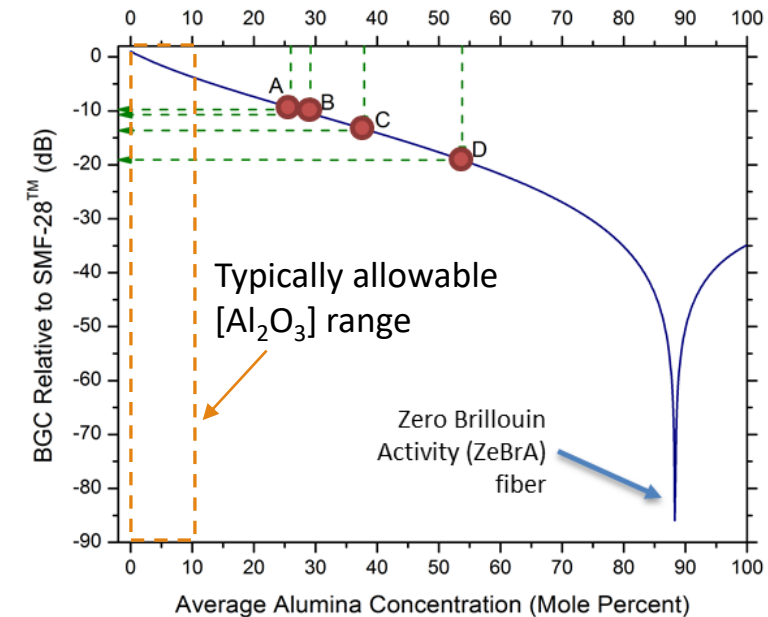
- Transverse photoelastic coefficients!

$$p_{12}^{\text{Al}_2\text{O}_3} < 0 \quad p_{12}^{\text{SiO}_2} > 0$$

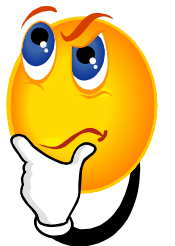
- Balance to greatly reduce Brillouin scattering; possibly negate completely!

$$\text{BGC} = \frac{2\pi n^7 p_{12}^2}{c\lambda^2 \rho V_a \Delta v_B}$$

- Measured BGC was ~100× lower than commercial single mode fiber.
- **Immensely useful: not just reduce... but completely eradicate SBS!**



What else now possible?



What's new about the BaO – SiO₂ system?

- Well... $p_{12}^{\text{BaO}} \sim 10 \times p_{12}^{\text{Al}_2\text{O}_3}$... but

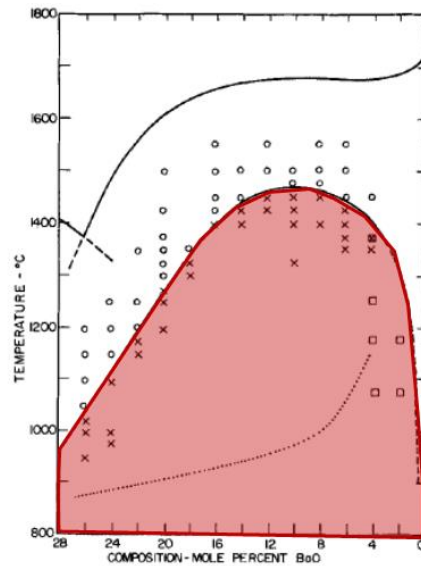
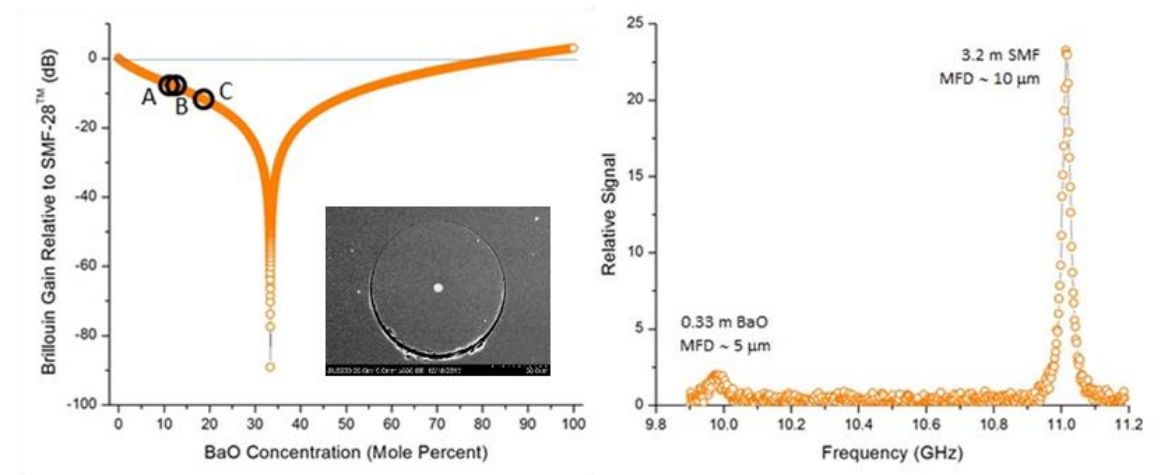


Fig. 2. Metastable miscibility gap in the system BaO-SiO₂. ○ = clear glasses, × = opalescent glasses, □ = electron microscope immiscibility data (no visible opalescence), dotted line = approximate temperatures below which samples could be held for 30 sec without visible opalescence.

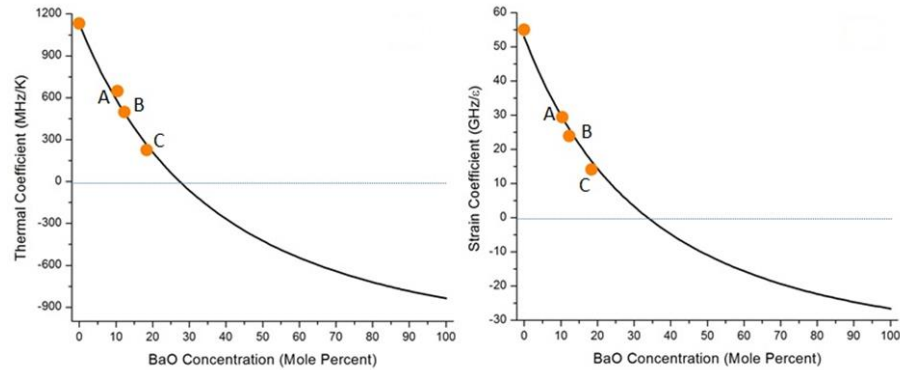
- Perfect for MCM since $T_m^{\text{BaO}} < T_{\text{draw}}^{\text{SiO}_2}$



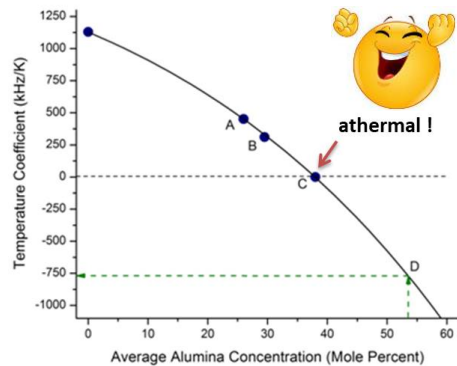
- This compositional balancing of + / - p_{12} greatly reduced Brillouin scattering. But can be done to other (selected) properties too!
- Counter-balancing thermo-acoustic and strain-acoustic coefficients yield *athermal and athermal Brillouin fibers*.

a-“X”-ic (atenstic, athermal) fibers

- BaO – SiO₂

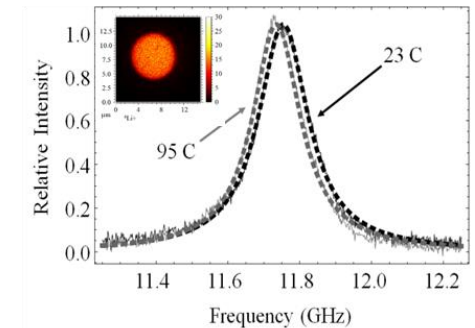
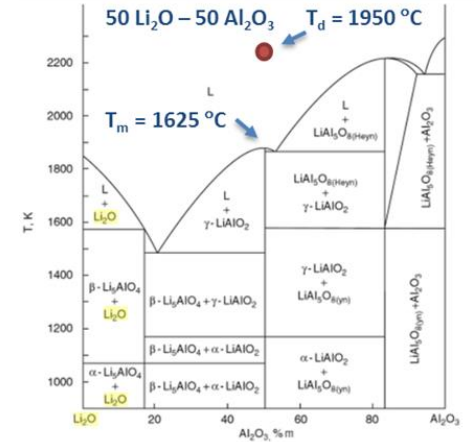


- Al₂O₃ – SiO₂



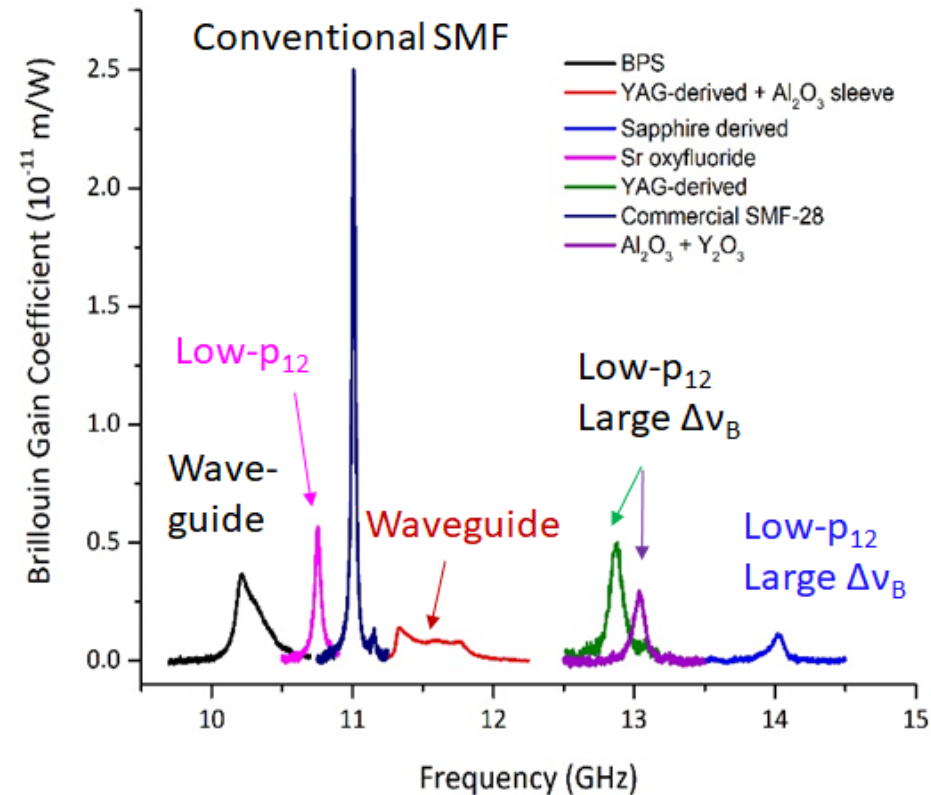
- Li₂O – Al₂O₃ – SiO₂

- $v_{\text{acoustic}}^{\text{SiO}_2}$ increases with increasing temperature but decreases with increasing pressure; SiO₂ is anomalous.
- Large core CTE relative to cladding, restricts thermal expansion; equivalent to a positive pressure.
- Increasing T (increasing v_A) increases pressure (decreasing velocity); which can cancel at the proper composition.
- Large CTE of Li₂O used as design parameter for a Brillouin-athermal single mode optical fiber.



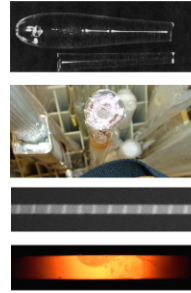
The Present...

- More compositions = more fun!
- Exploration of novel phenomena, such as intrinsically low ($< \text{SiO}_2$) multicomponent glass fibers.
- Can make fiber perform in ways never thought possible or permissible by design alone.
- But there's more!!!



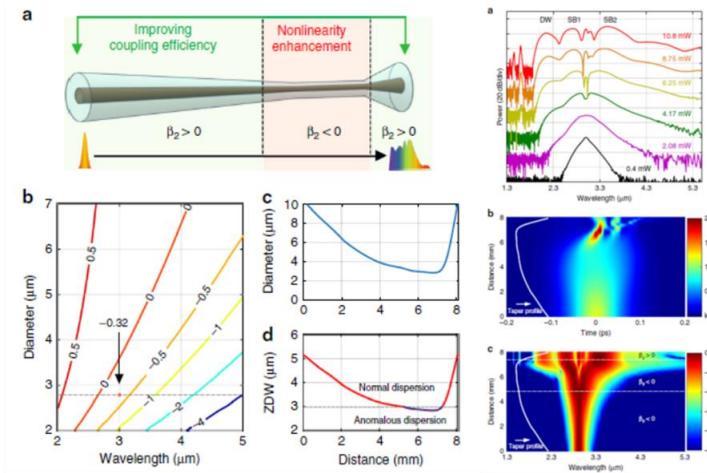
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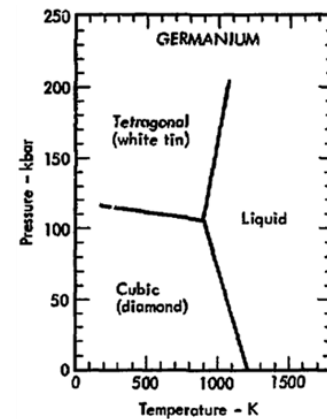
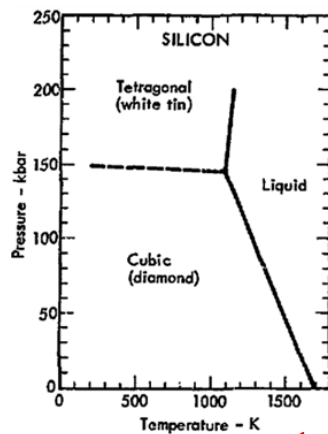
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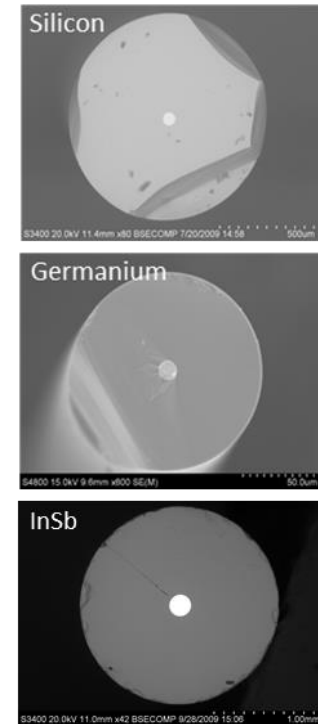
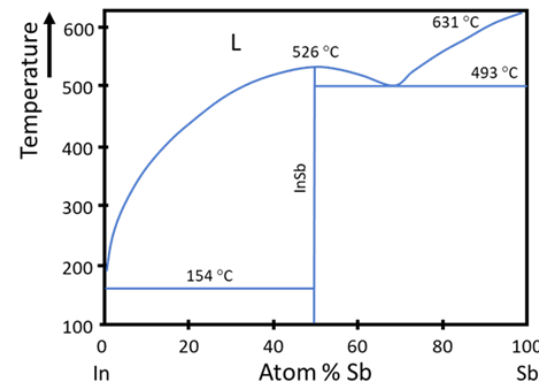
- Compact SCF platform achieves low loss transmission across the mid-IR spectral regime. Exploiting a novel asymmetric taper design, coherent SC span of 1.74 octaves was generated from 1.6 to 5.3 μm , which is the broadest SC reported in a silicon core/silica-clad waveguide.

The role of phase diagrams...

- **Optical fibers are (normally) made of glass... why consider (equilibrium) phase diagrams?**
 - Phase diagrams can inform dopant / additive solubility limits AND glass forming compositions.
- **For crystalline core fibers, they are invaluable...But not always appreciated...**
 - **Gen 0** (2008 – 2010): Unary, e.g., **Si** and **Ge**, and line compounds, e.g., **InSb** and **GaSb**... phase diagrams inform melting points, phase transitions, and phases immediately off stoichiometry.

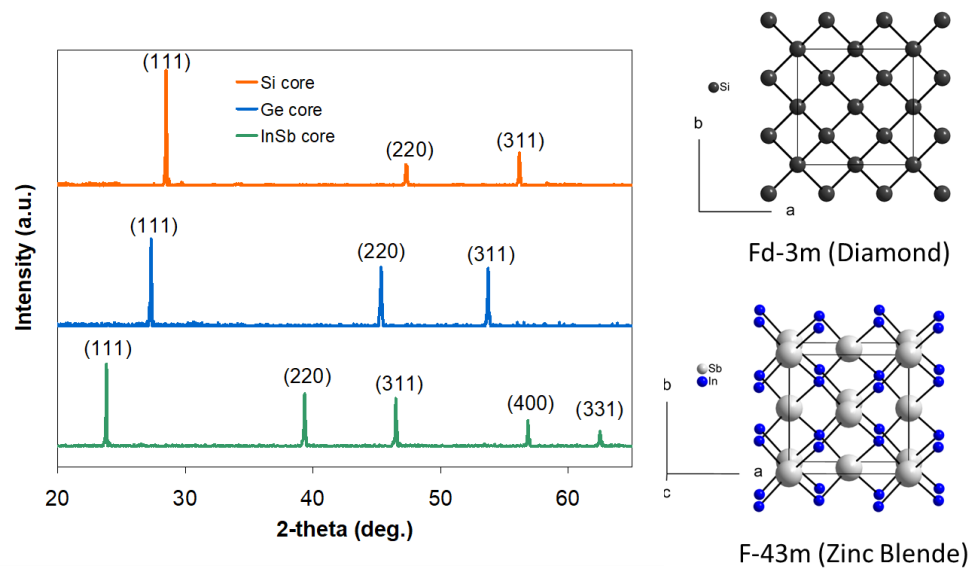


1 atm = 0.001 kbar



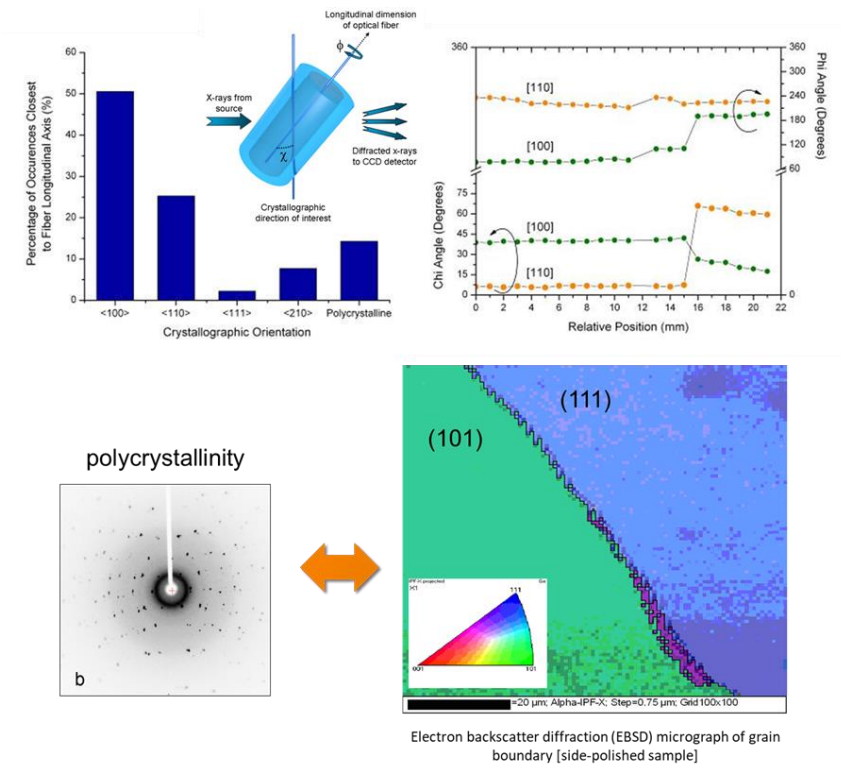
Gen 0: Unary phases and line compounds

- As drawn... highly crystalline!! **But polycrystalline.**



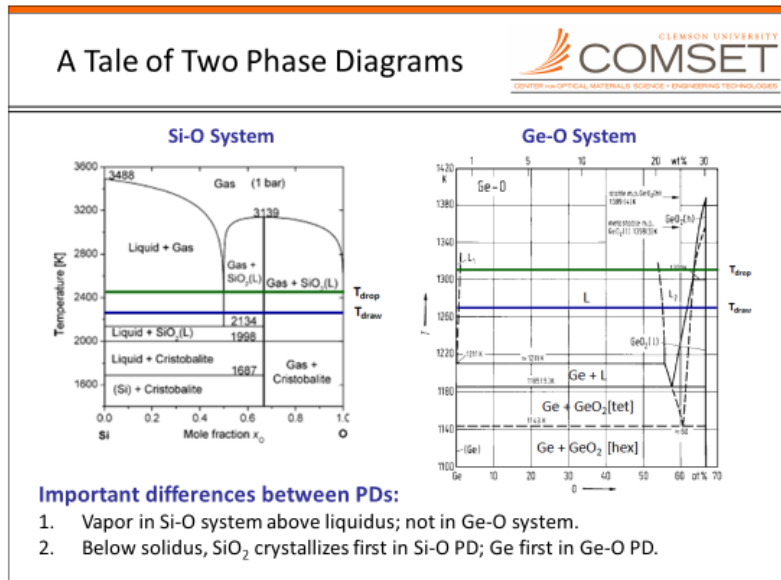
- N.B.:* Crystalline nature of cores implies equilibrium processes despite high draw speeds. In reality, kinetics of crystallization of semiconductors from melt extremely fast.

Over longer distances (> cm), the orientation is found to change along length of fiber so technically poly-crystalline but with large grain size in comparison to fiber dimensions (> 1000:1).

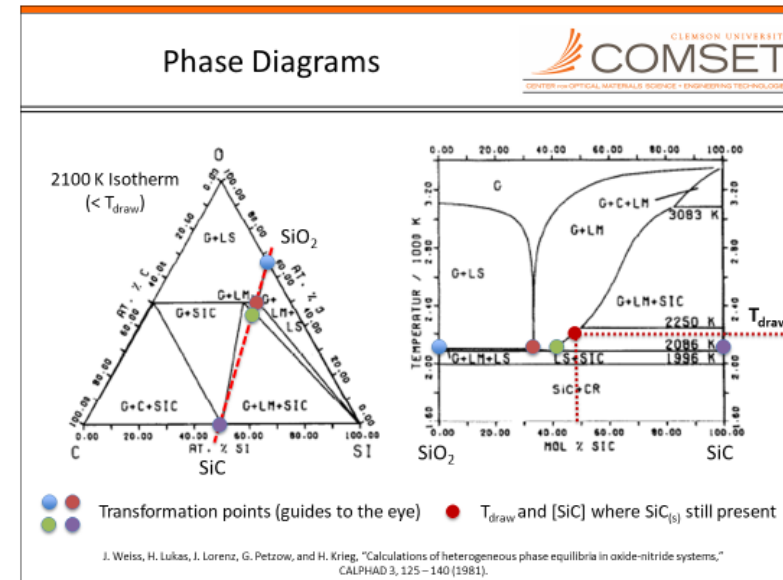


Gen 1: Reactive molten core

- **Gen 1** (2011)... used only for managing oxygen contamination.
 - Understand the Si-O and Ge-O systems (did help realize zero oxide content Ge:SiO₂ fibers)
 - Taught oxygen gettering by reactive molten core: SiO₂ + SiC → Si + SiO_g + CO_g.
 - MCM permits *in-situ* chemistry! Will be very important later...



S. M. Schnurre, J. Gröbner, and R. Schmid-Fetzer, "Thermodynamics and phase stability in the Si-O system," *J. Non-Cryst. Solids* **336**, 1–25 (2004).
 F. Trumbore, C. Thurmond, and M. Kowalchik, "Germanium-oxygen system," *J. Chem. Phys.* **24** 1112 (1956).



J. Weiss, H. Lukas, J. Lorenz, G. Petzow, and H. Krieg, "Calculations of heterogeneous phase equilibria in oxide-nitride systems," *CALPHAD* **3**, 125–140 (1981).
 S. Morris, T. Hawkins, P. Foy, C. McMillen, J. Fan, L. Zhu, R. Stolen, R. Rice, and J. Ballato, "Reactive Molten Core Fabrication of Silicon Optical Fiber," *Optical Materials Express* **1**, 1141–1149 (2011).

Gen 1.5: Reactive (interfacial) molten core

- **Gen 1.5** (2013)... still used only for managing oxygen contamination... but better...
 - Interfacial modifiers... based on CaO – SiO₂... silicon / slag literature...
 - Critical advance in achieving long lengths of oxygen-free silicon core fibers.

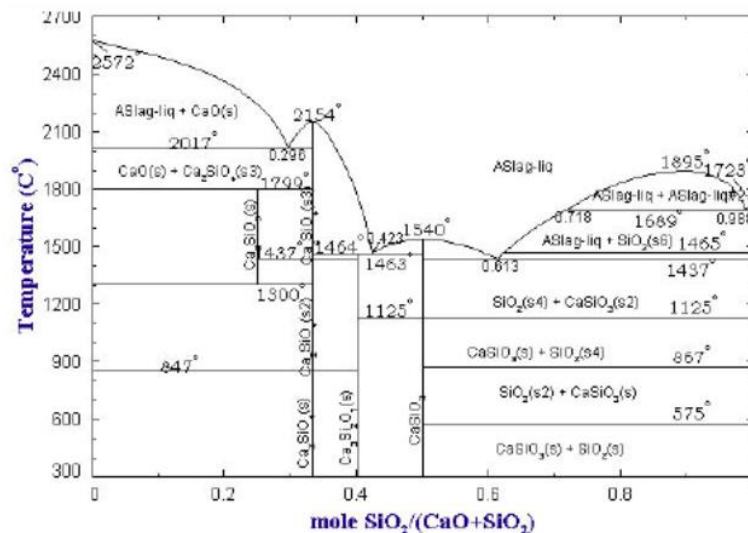
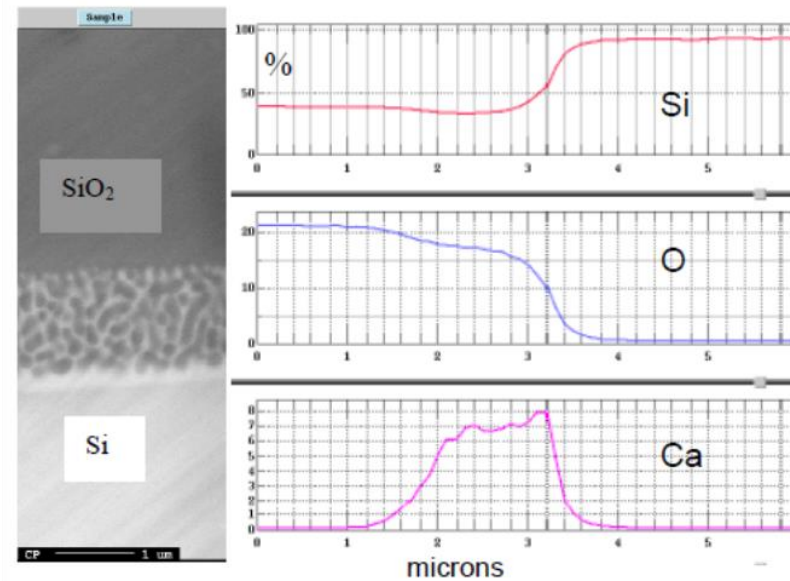


Fig. 2 Phase diagram of the CaO – SiO₂ system [20]



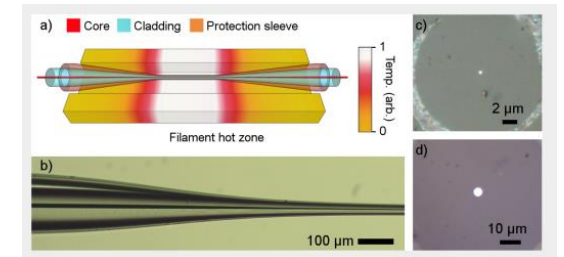
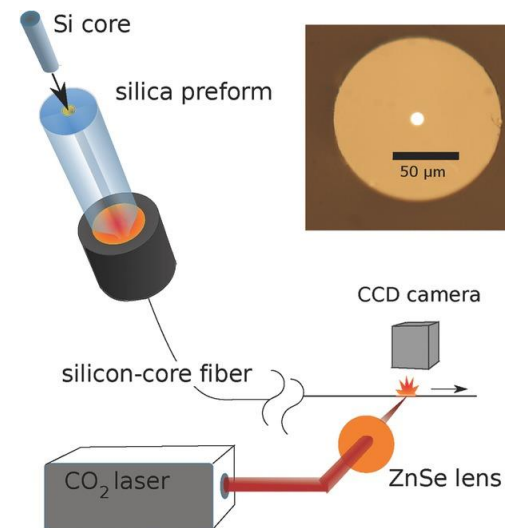
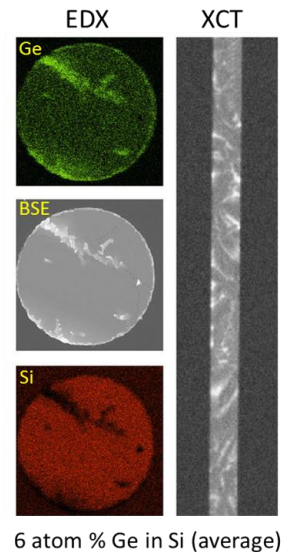
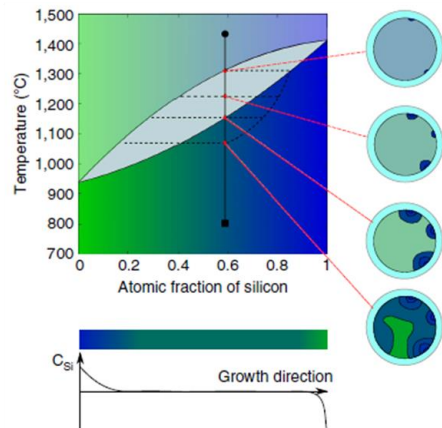
Gen 2: Isomorphous molten core...

- **Gen 2** (2016)... Two critical advances:

1. **Isomorphous systems**, e.g., Si-Ge.

2. **Laser post-processing** to zone recrystallize / repurify and create in-fiber structures and tapers.

As-drawn fibers have compositional variations due to non-equilibrium cooling.

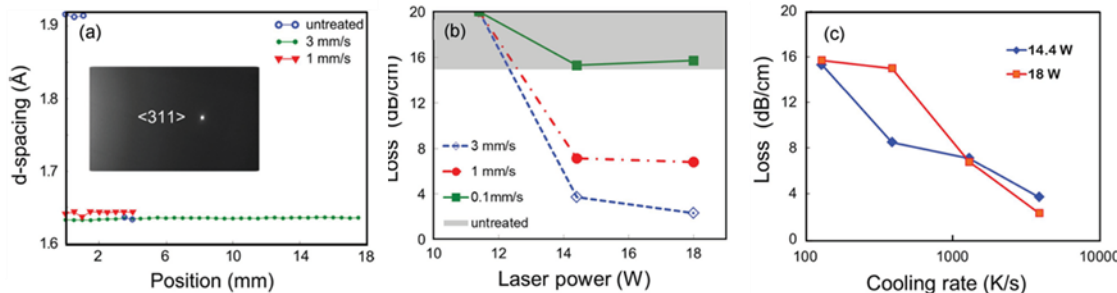


Gen 2: Isomorphous molten core... and laser post-processing

2. Laser post-processing to zone recrystallize / repurify and create in-fiber structures and tapers.

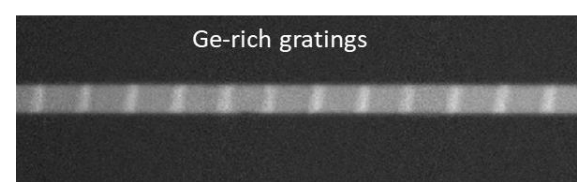
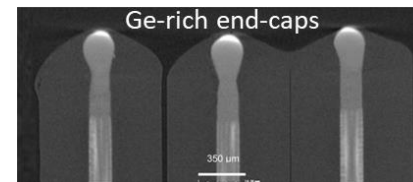
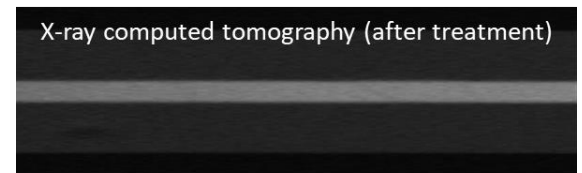
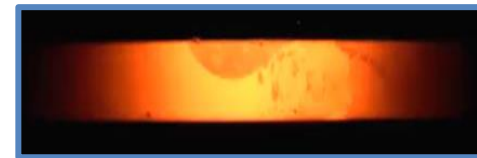
Example 1: Si

- High speed translational annealing: establish melt zone, translate fiber.
- Nucleation suppressed, single crystalline over entire length and preferential segregation of impurities.
- Loss reduction, now routinely ~ 0.1 dB/cm.



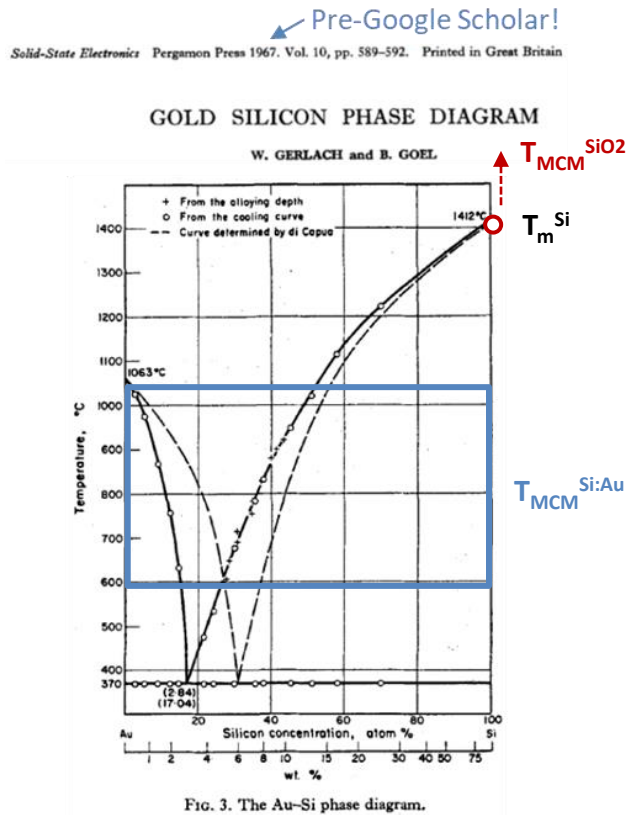
Example 2: Si-Ge

- Ge-rich material accumulates in the high temperature region.
- Establish melt zone – translate through fiber. Competition between nucleation suppression and unstable growth front.



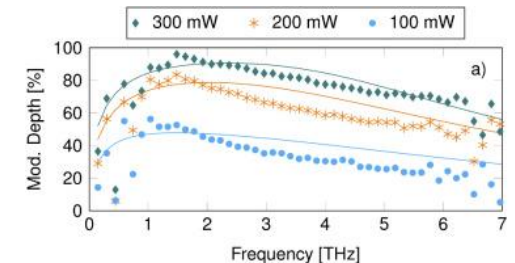
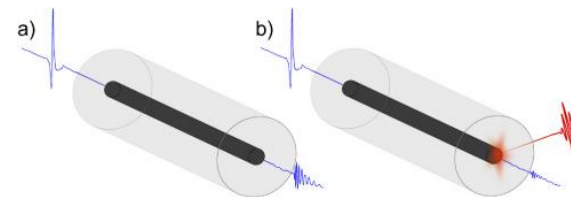
Gen 3: Eutectic molten core...

- **Gen 3** (2018)... Eutectic systems



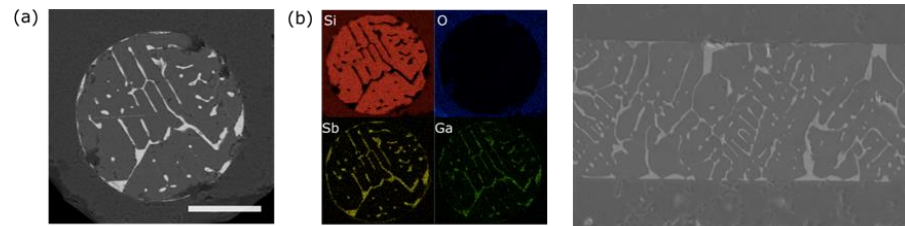
- e.g., eutectic Si-Au system

- Draw homogeneous mixture in eutectic region, spatially post-process below melting point of either end-member, and then transition (L + S) field to solidify desired phase.
- Facilities low temperature fabrication, less contamination, AND better zone refinement / recrystallization.
- Employed for high-speed all-optical modulation of broadband THz signals within a SCF with low levels of gold.

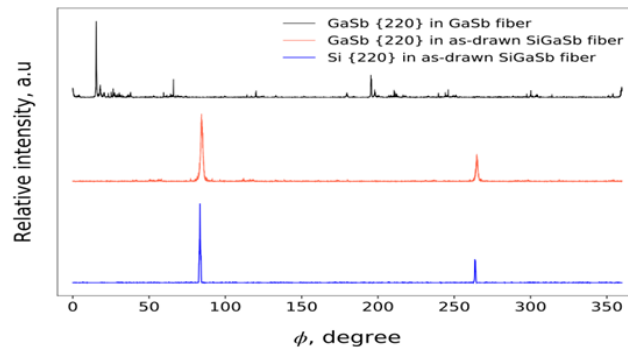


Gen 3: Eutectic molten core...

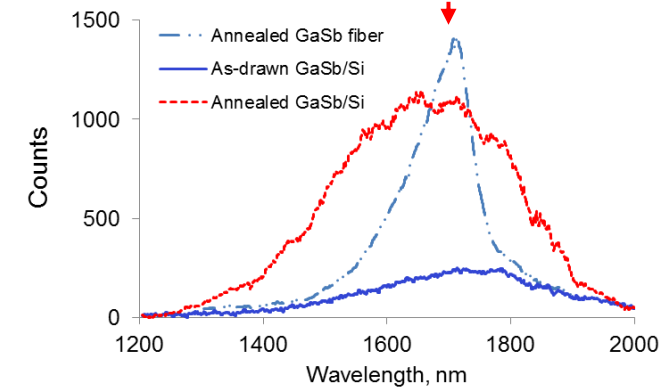
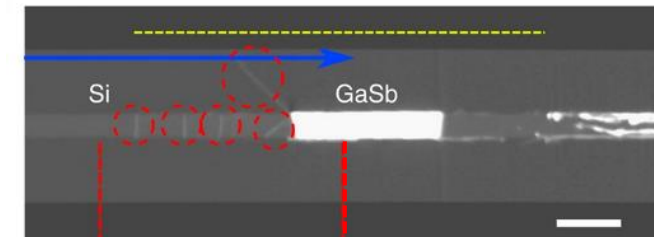
- **Gen 3** (2018)... Eutectic systems
 - e.g., Si and III-V core: GaSb as solvent



- Heterogeneous as-drawn fiber but with Si / GaSb phases co-aligned.

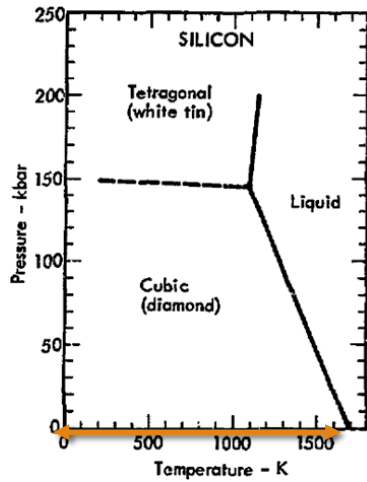


- Laser post-processing...

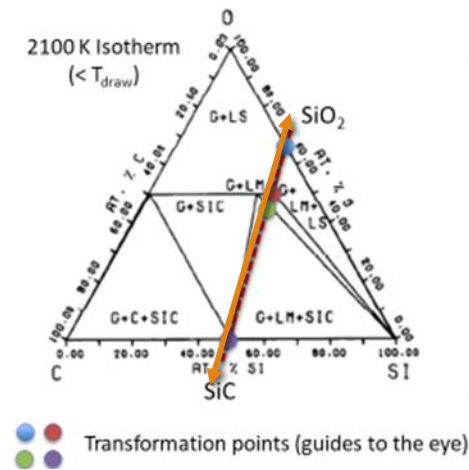


The role of phase diagrams... becoming more appreciated

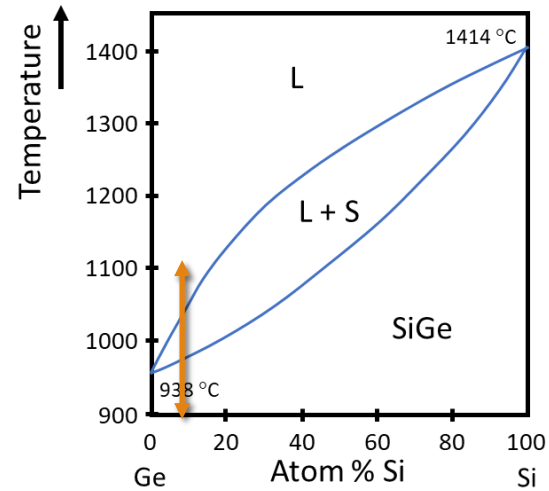
Gen 0
(2008)



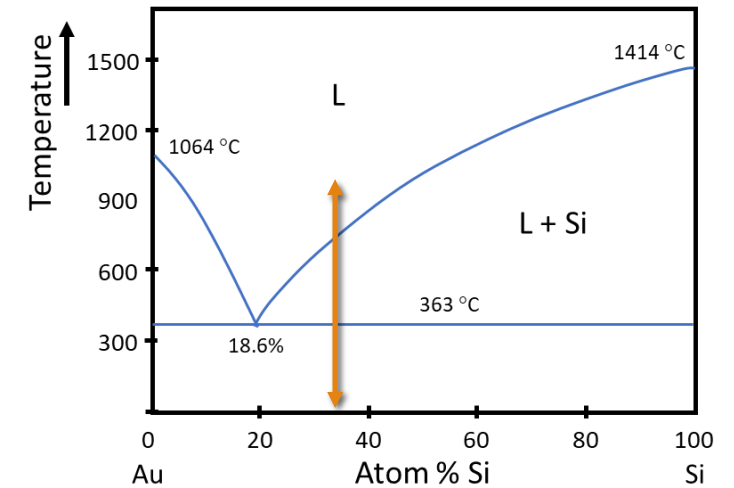
Gen 1
(2011)



Gen 2
(2016)

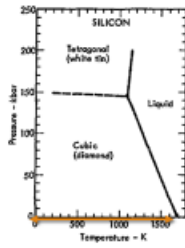


Gen 3
(2018)

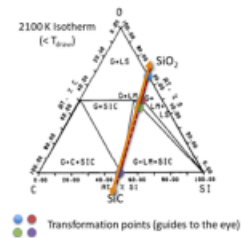


The role of phase diagrams... becoming more appreciated

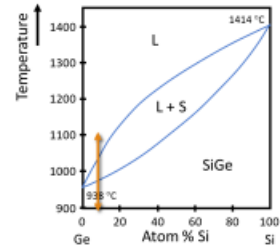
Gen 0
(2008)



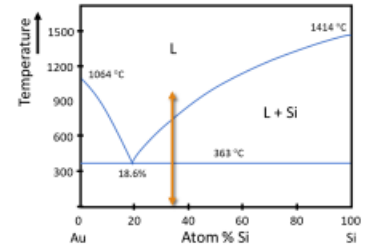
Gen 1
(2011)



Gen 2
(2016)



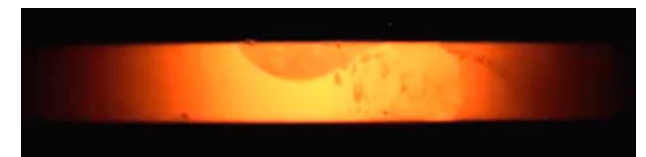
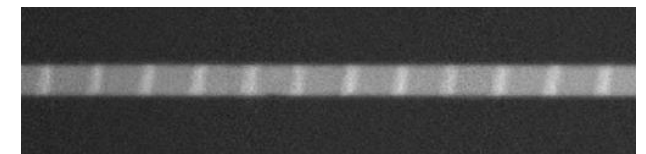
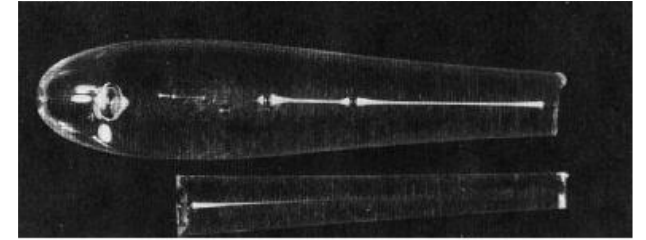
Gen 3
(2018)



Gen 4
(2022...)



-
- How did we get here?
 - Where's here?
 - No. No. No. Maybe. OK. Boom. Whoa.
 - What's next?!?!

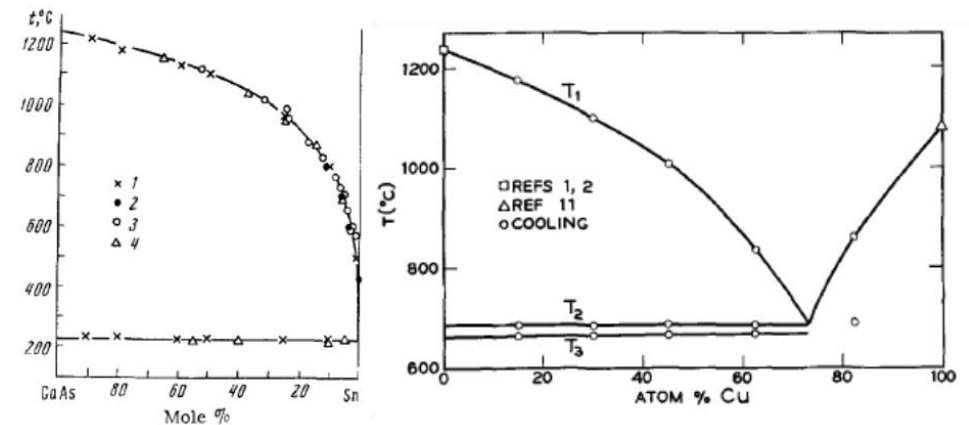


The **FUTURE** ... doing the impossible...



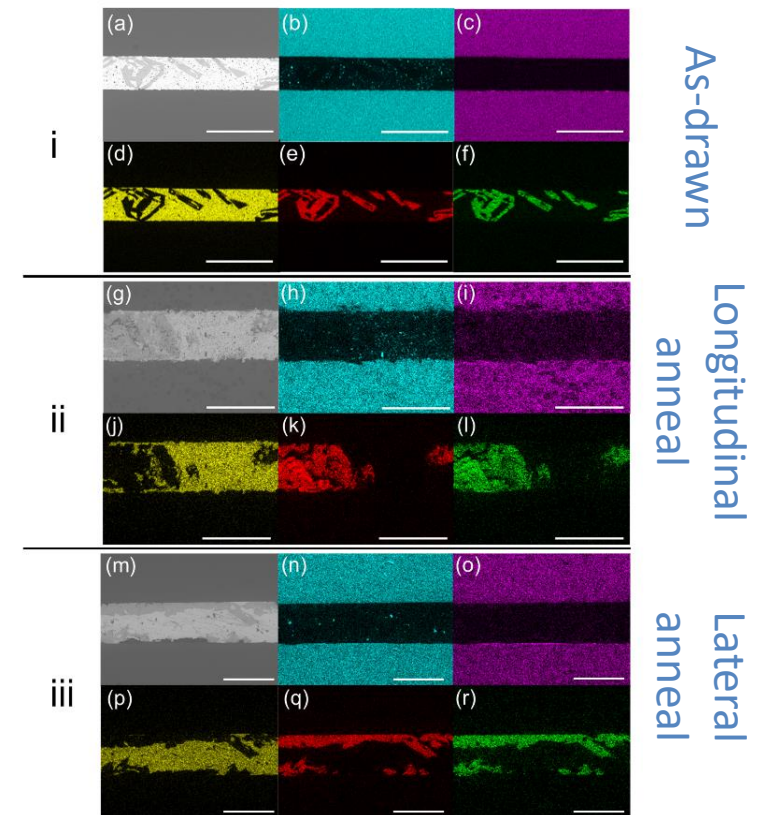
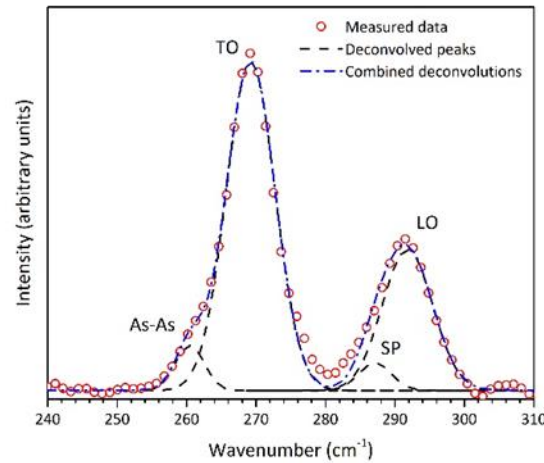
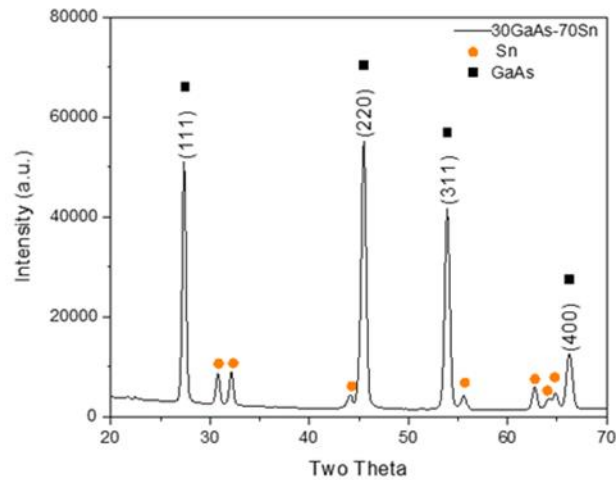
- **Gen 4 (now!)**
 - Established that the molten core is limited to phases exhibiting low / no vapor pressure at the melting point...

- **But...**
 - Volatility depends on temperature, which can be greatly reduced using the now-established flux approaches!



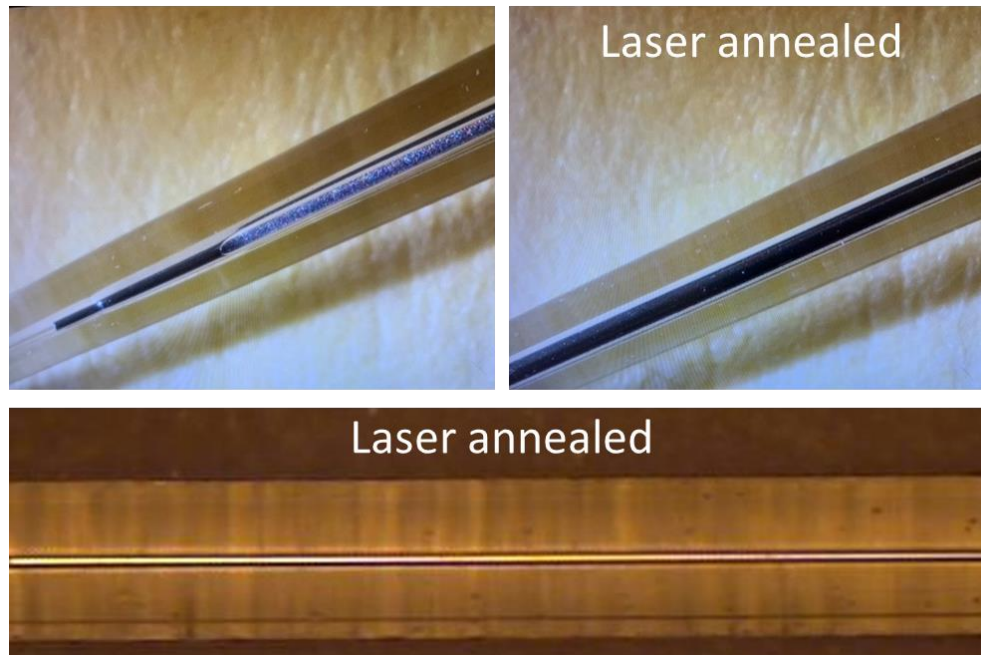
Gen 4: Flux molten core...

- **Gen 4** (2022)... Volatile and incongruent melting cores, e.g., GaAs.
- E.g., GaAs core optical fiber!
 - $T_m = 1245^\circ\text{C}$... but very high VP...
 - Use fluxes to reduce liquidus and apply MCM below where volatility is problematic.



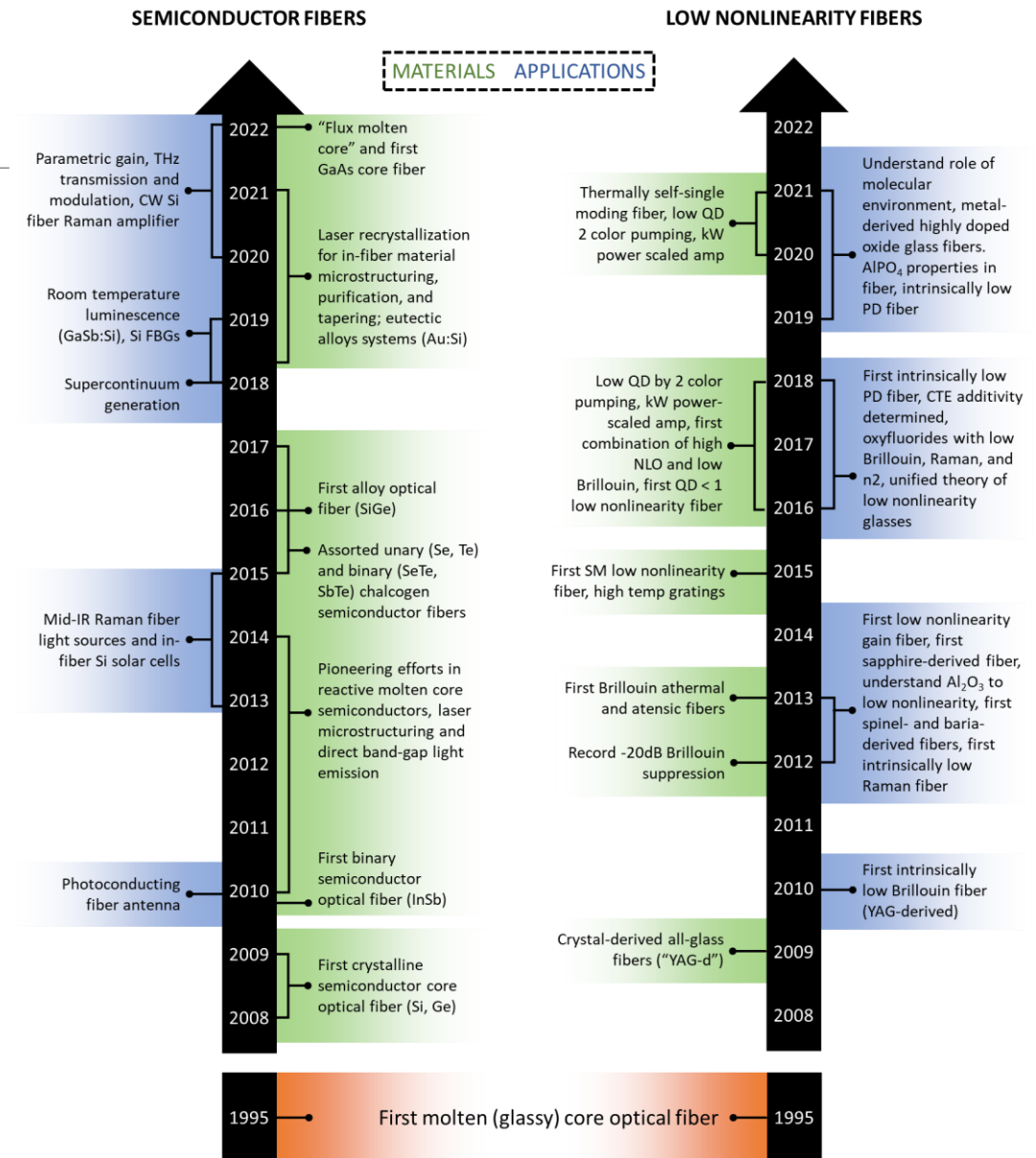
Gen 4: Flux molten core...

- **Gen 4** (2022)... Volatile and incongruent melting cores, e.g., GaAs.
 1. **Laser annealing and segregation.**
 2. **Scalable:** 100 m of the as-drawn, DURAN® glass-clad, crystalline 30GaAs-70Sn core fiber.



Conclusions... for now!

- The molten core method has opened the periodic table to advanced and multi-functional fibers.**
 - Commercially scalable; all sorts of fun, useful, and novel glass and crystal science!
 - Only process that yields amorphous and crystalline core fibers (depending on material family) over long lengths at practical speeds.
 - Employed globally (77 countries to-date) for the study and use of a wide range of novel in-fiber photonic and opto-electronic devices.



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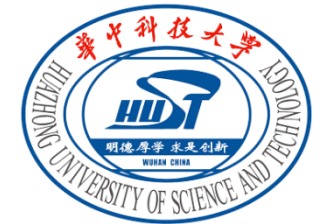


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Thank You !!

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