

Ultrafast Dynamics and Precision Stabilization in Chip- Scale Optical Frequency Combs

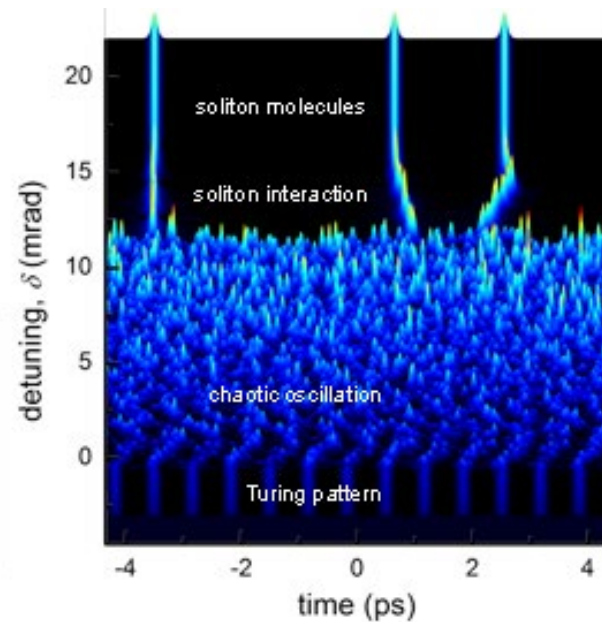
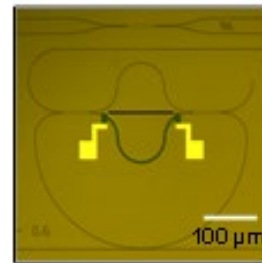
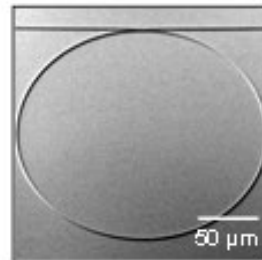
Presented by:



Welcome to Today's Webinar

"Ultrafast Dynamics and Precision Stabilization
in Chip-Scale Optical Frequency Combs"

Dr. Shu-Wei Huang, UCLA



Technical Group Committee



Kensuke Ogawa
Fujikura
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Contact the Committee for an opportunity as a Social Media Officer.

Scope of the Technical Group

- The integration of optical components to perform various functions such as WDM, optical signal processing, etc.
 - Technology platforms
 - Compound semiconductor photonics
 - Silicon photonics
 - Polymer photonics

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Integrated Optics (PI)

www.osa.org/IntegratedOpticsTG

- TG members involved as session co-chairs in the upcoming meetings



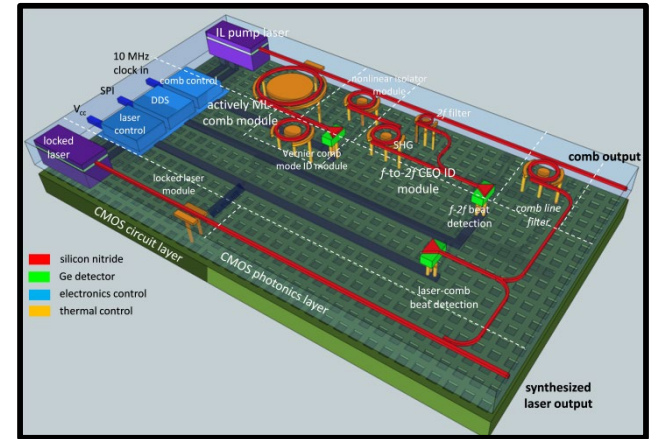
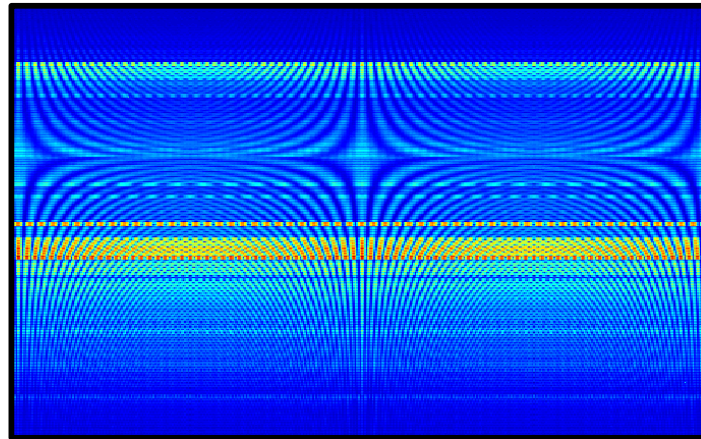
The 24th Congress of
the International Commission for Optics

Date 21 (Mon) - 25 (Fri) August 2017

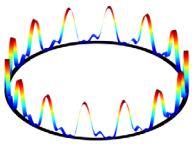
Venue : Keio Plaza Hotel, Tokyo

Get involved with your suggestion of invited speaker candidates!

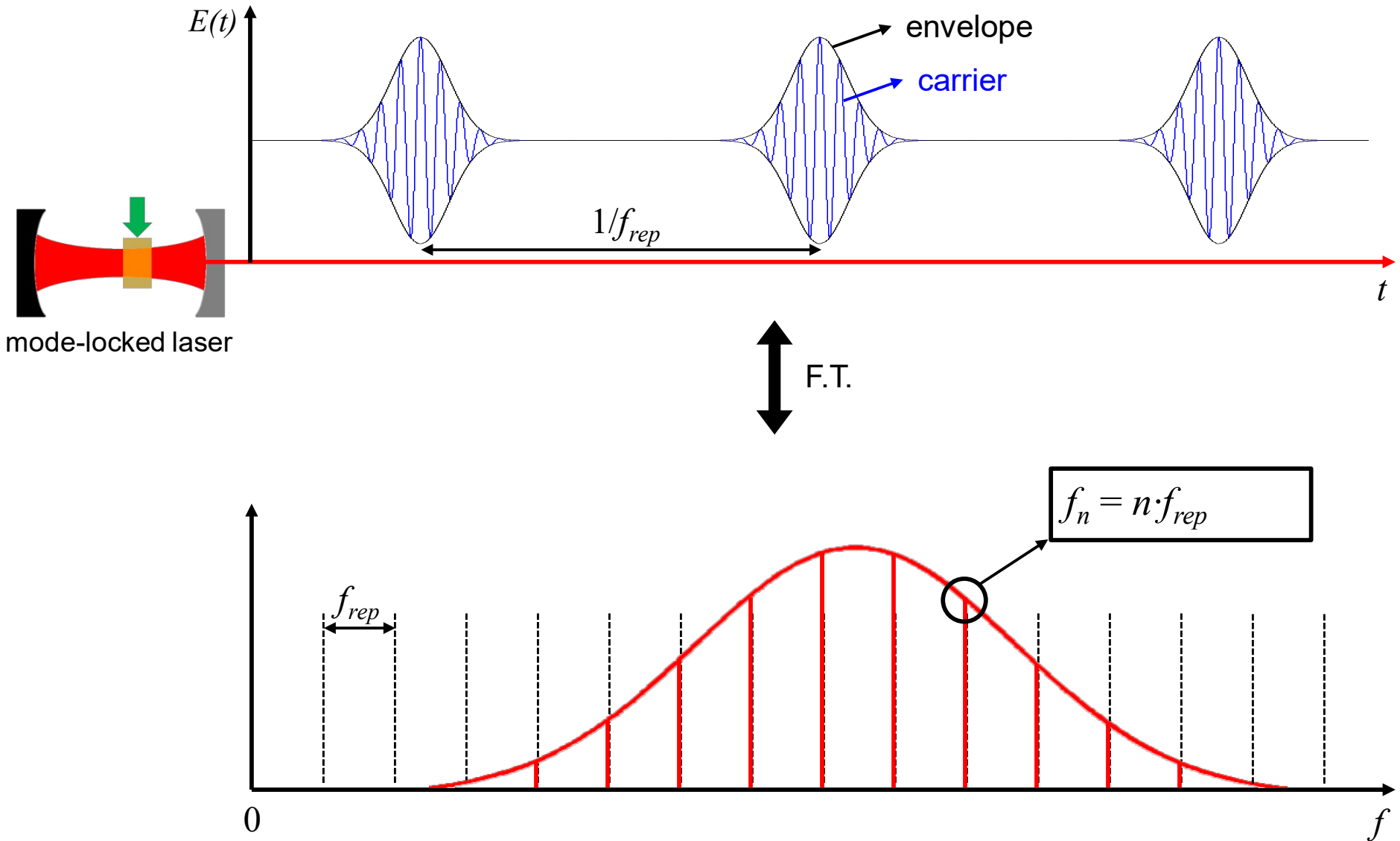
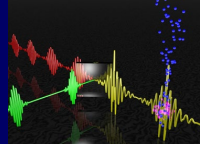
Ultrafast dynamics and precision stabilization in chip-scale optical frequency combs

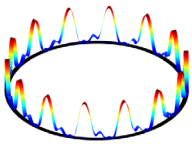


Shu-Wei Huang
University of California Los Angeles

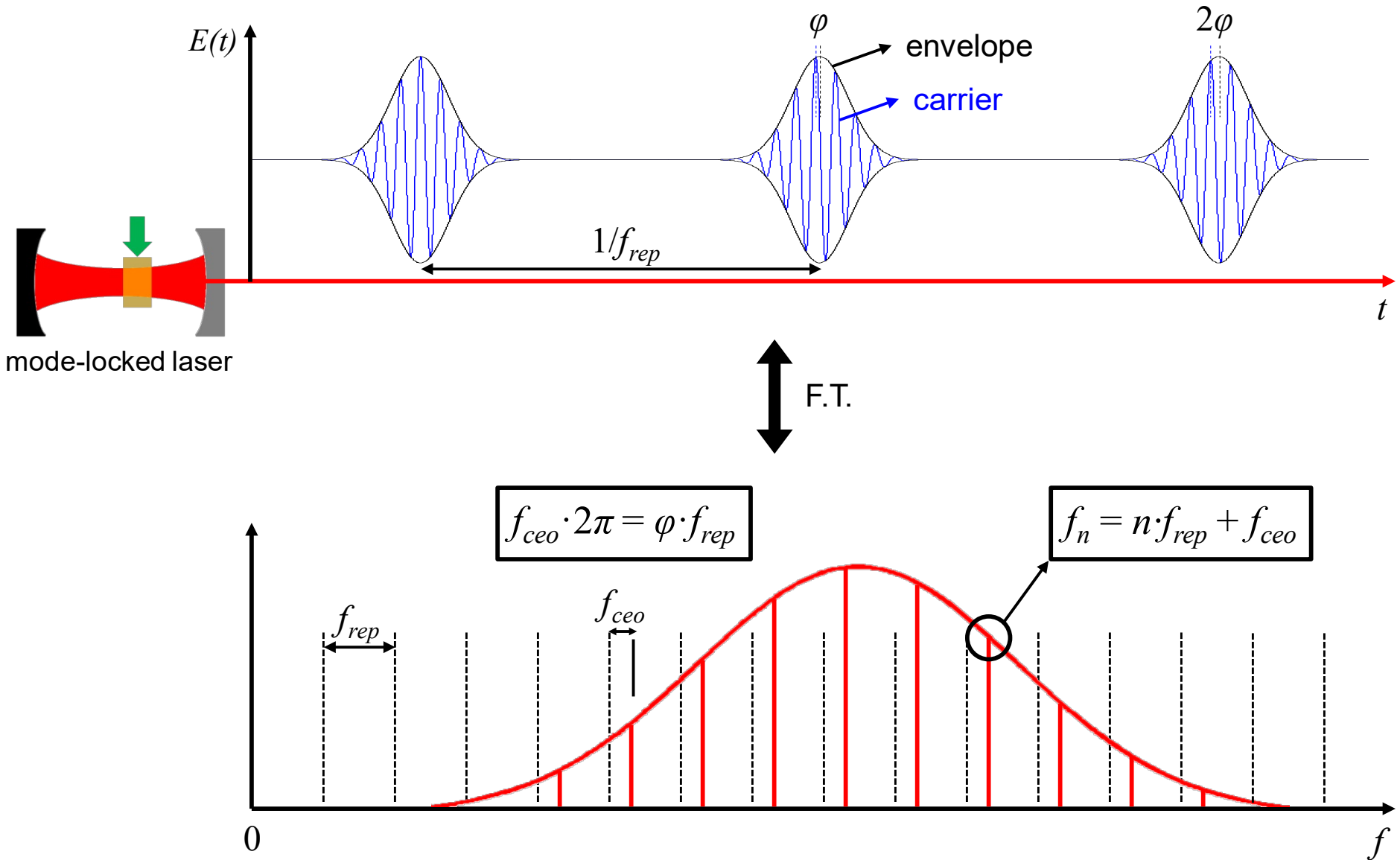
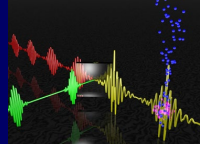


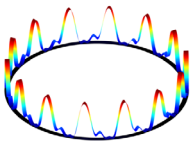
Optical Frequency Comb



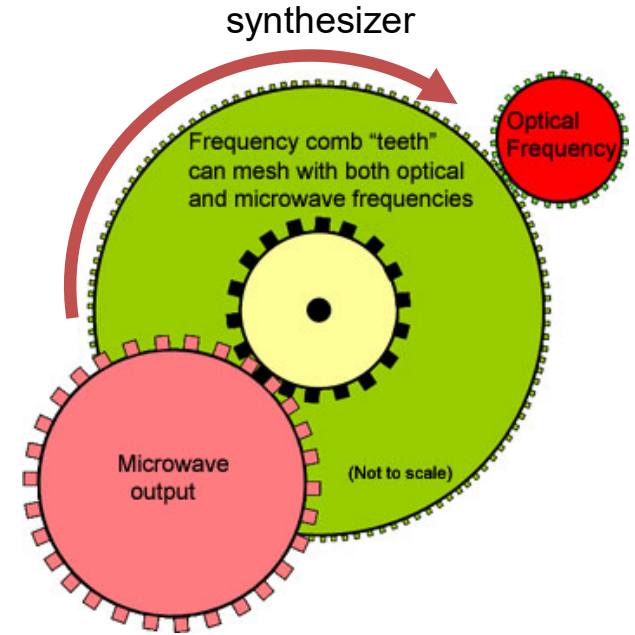
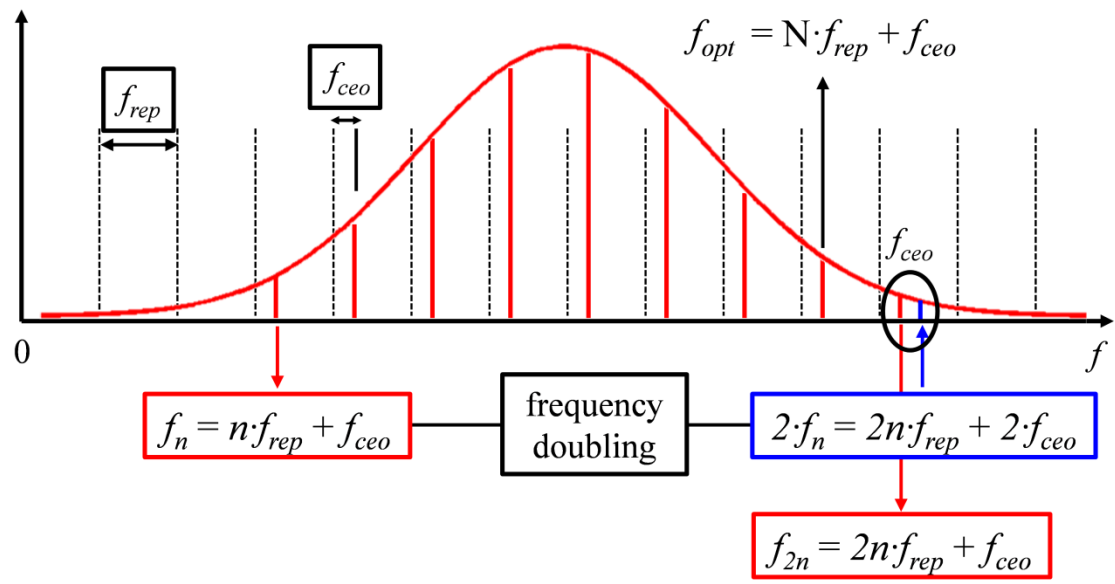
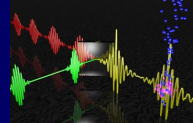


Optical Frequency Comb





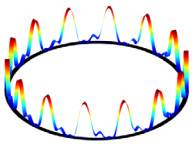
An elegant way to link electronics with optics



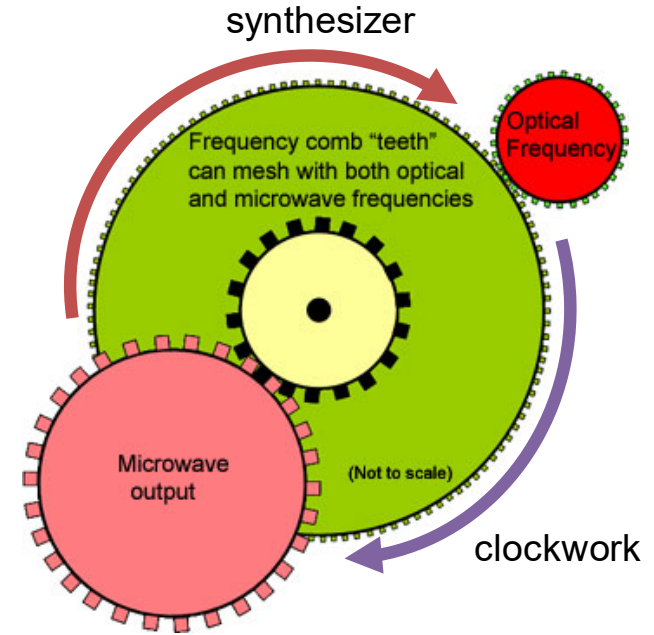
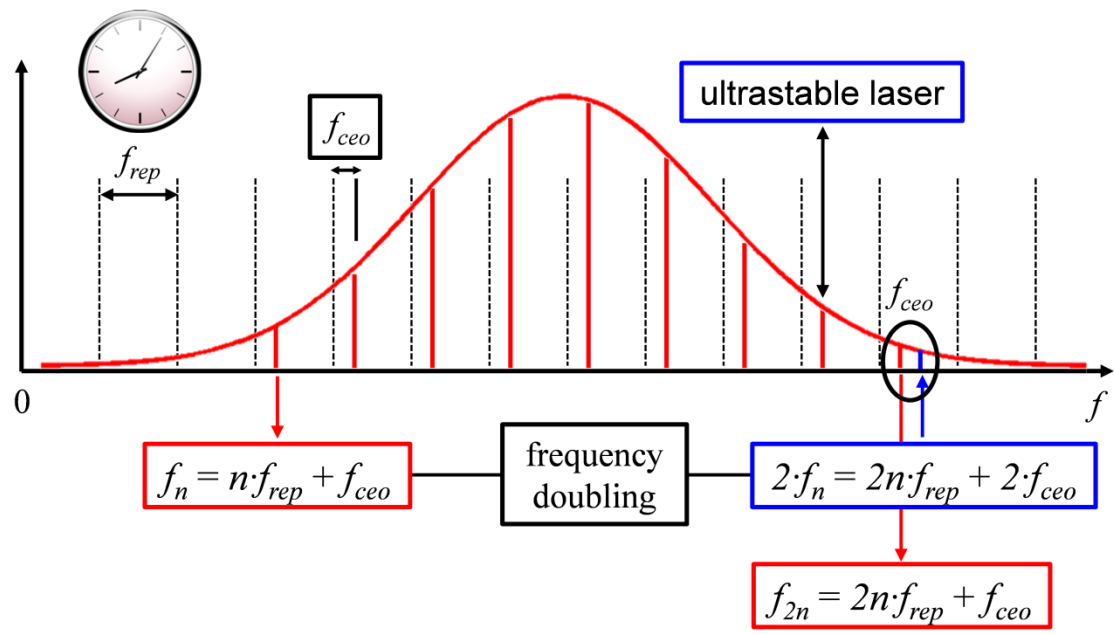
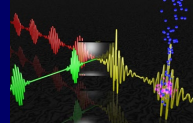
NIST

1. Locking both f_{rep} and f_{ceo} to electronic oscillators leads to accurate evaluation of optical frequencies.



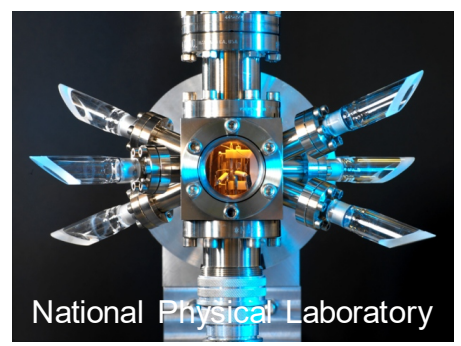


An elegant way to link electronics with optics



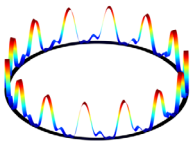
1. Locking both f_{rep} and f_{ceo} to electronic oscillators leads to accurate evaluation of optical frequencies.
2. Locking f_{opt} to an ultrastable laser and f_{ceo} to an electronic oscillator lead to the next time standard.

NIST

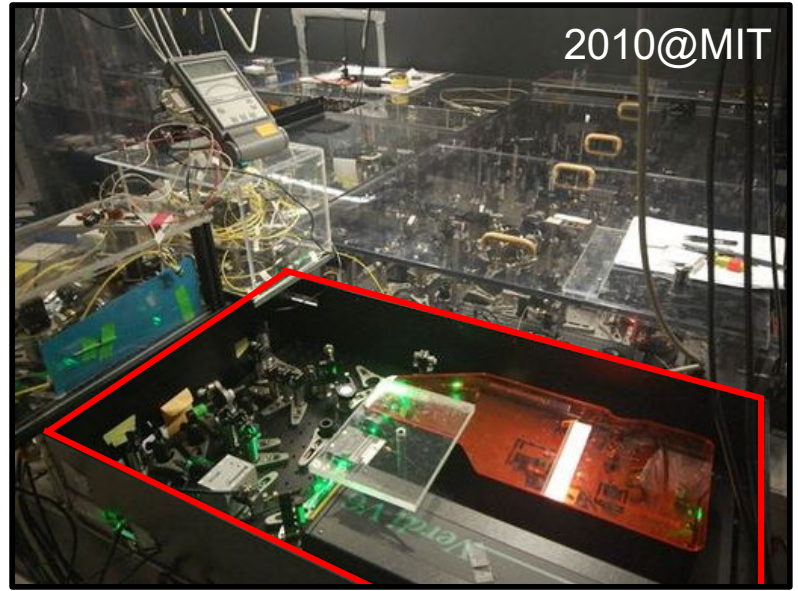
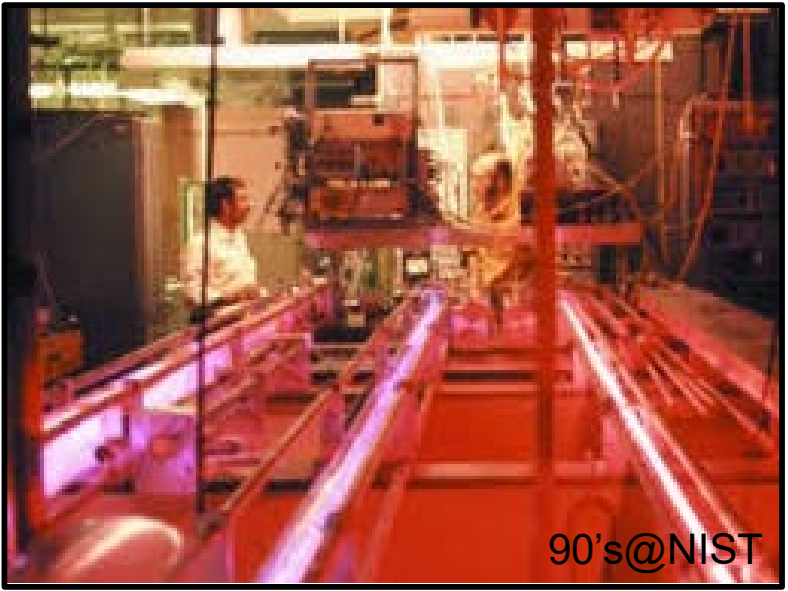
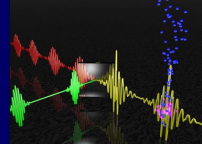


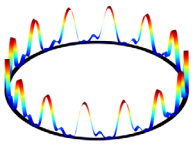
National Physical Laboratory



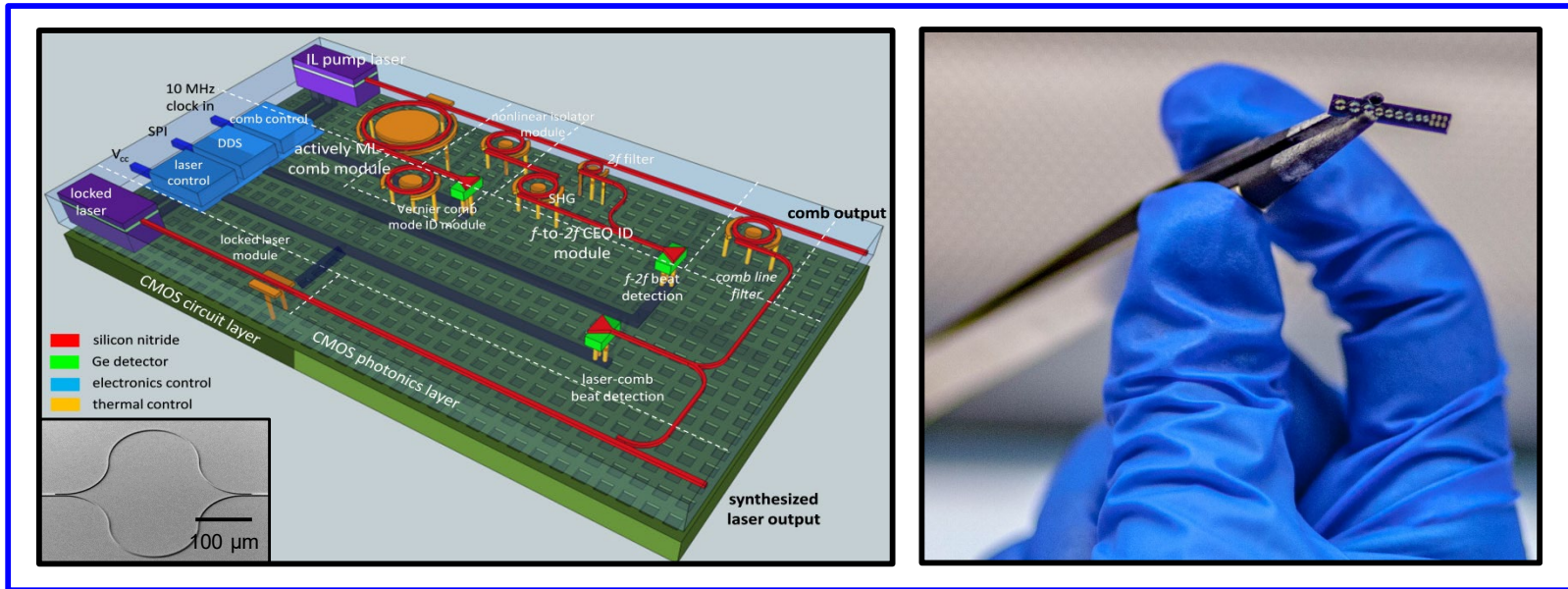
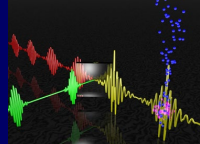


Frontier of frequency metrology



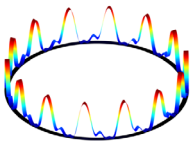


Chip-scale Optical Frequency Comb

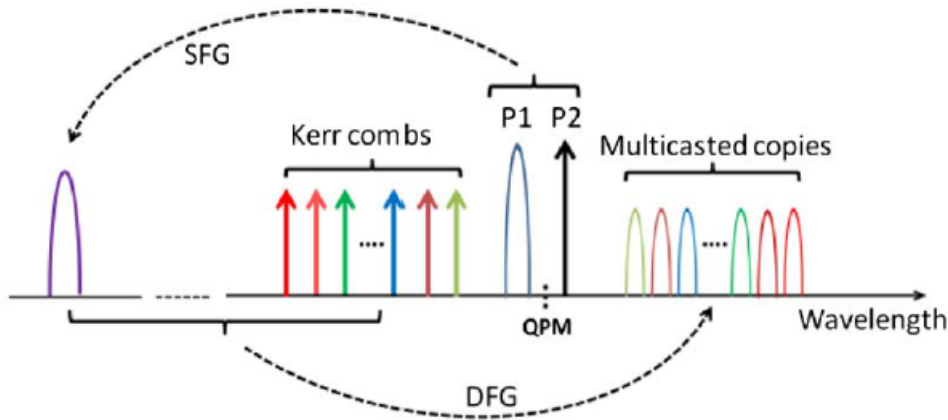
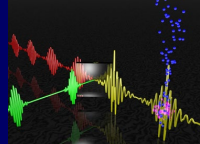


1. Microresonator-based ultrafast light source delivering 74 femtosecond pulse train
- Huang *et al.*, *Phys. Rev. Lett.* **114**, 053901 (2015).
2. Low noise broadband microcomb containing 3,600 coherent frequency teeth
- Huang *et al.*, *Sci. Rep.* **5**, 13355 (2015).
3. High bandwidth comb stabilization achieving a fractional uncertainty of 2.7×10^{-16}
- Huang *et al.*, *Sci. Adv.* **2**, e1501489 (2016).
4. Microresonator stabilized diode laser at the thermodynamical limit of 1.7×10^{-13}
- Lim *et al.*, *Opt. Lett.* **41**, 3706 (2016).





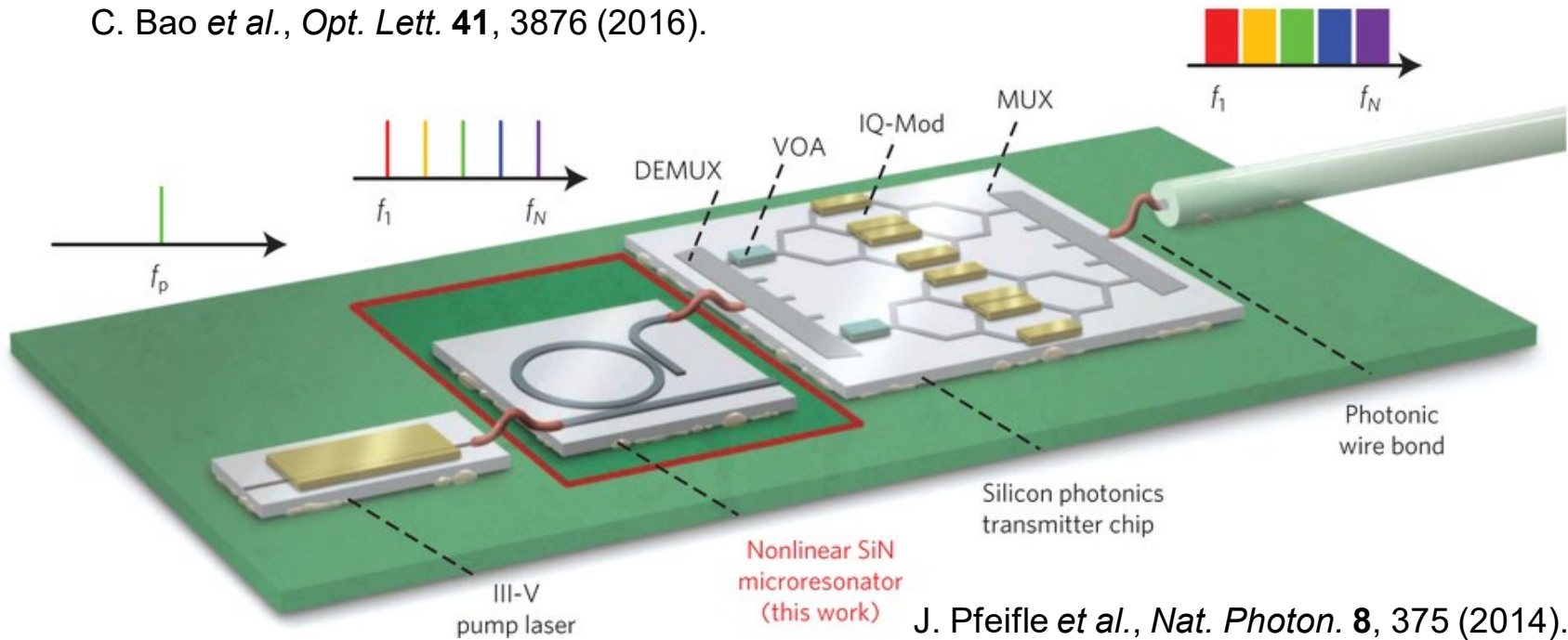
Terabit optical telecommunications



$\lambda_1 \lambda_2 \lambda_3 \lambda_4$

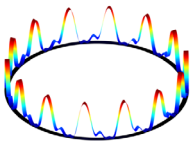
“The combination of chip-scale Kerr frequency comb sources with large-scale silicon photonic integration can become a key concept for power-efficient optical interconnects.”

C. Bao *et al.*, *Opt. Lett.* **41**, 3876 (2016).

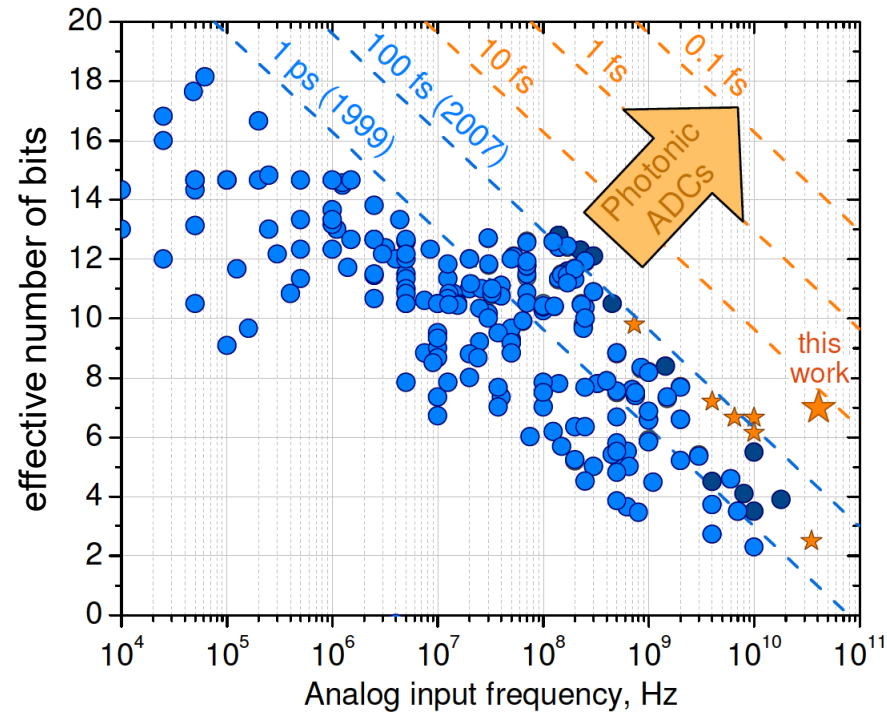
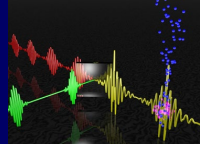


J. Pfeifle *et al.*, *Nat. Photon.* **8**, 375 (2014).

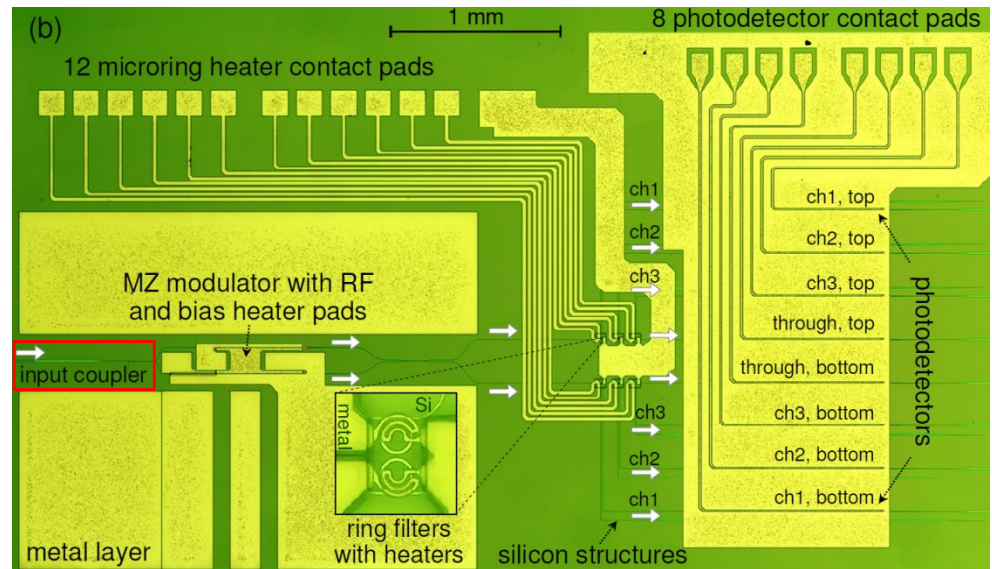
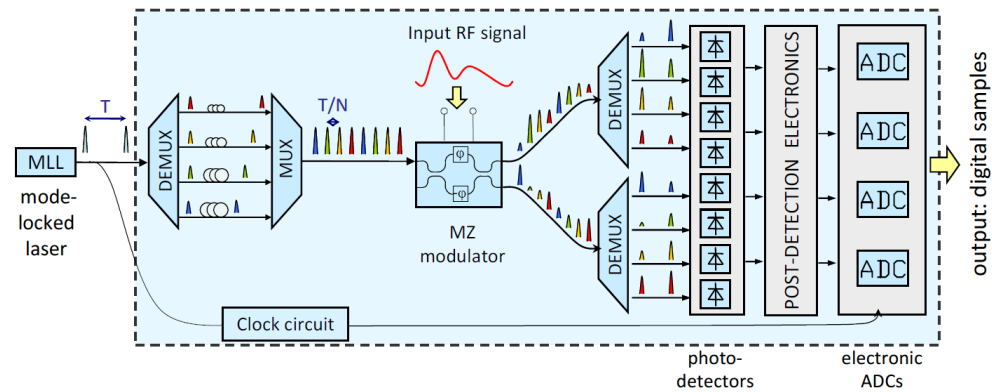




Photonic analog-digital converter

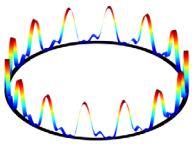


Sampling microwave signals directly in the optical domain with mode-locked lasers has shown promises to overcome the bottleneck of aperture jitter in the high-speed and high-resolution ADCs.

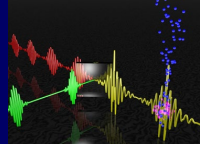


A. Khilo *et al.*, *Opt. Express* **20**, 4454 (2012).

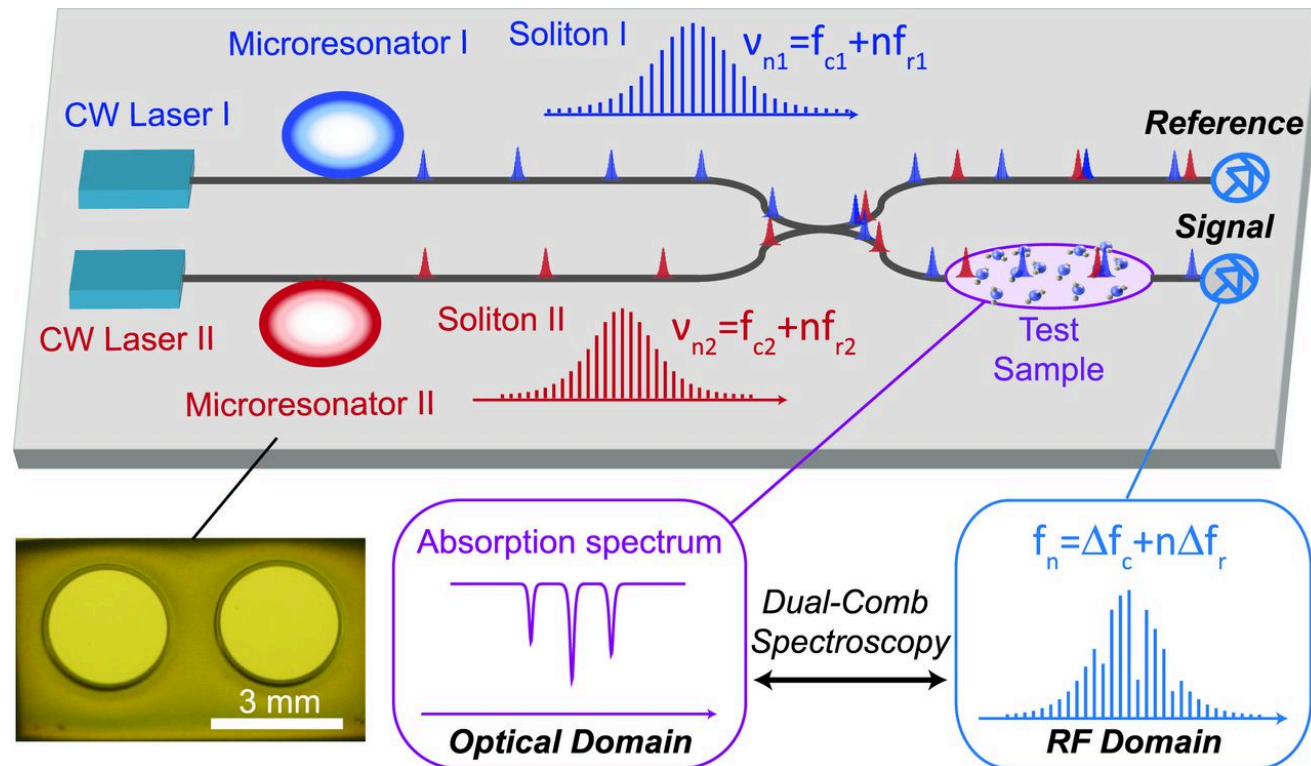




Chip-scale dual-comb spectroscopy

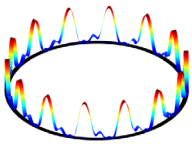


“The integration with other devices makes chip-scale Kerr frequency comb sources well suited for possible realization of a dual-comb spectroscopic system-on-a-chip.”

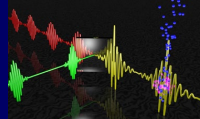


M.-G. Suh *et al.*, *Science* **354**, 600 (2016).





Astro-comb for earth-like exoplanet search



Harvard-Smithsonian Center for Astrophysics

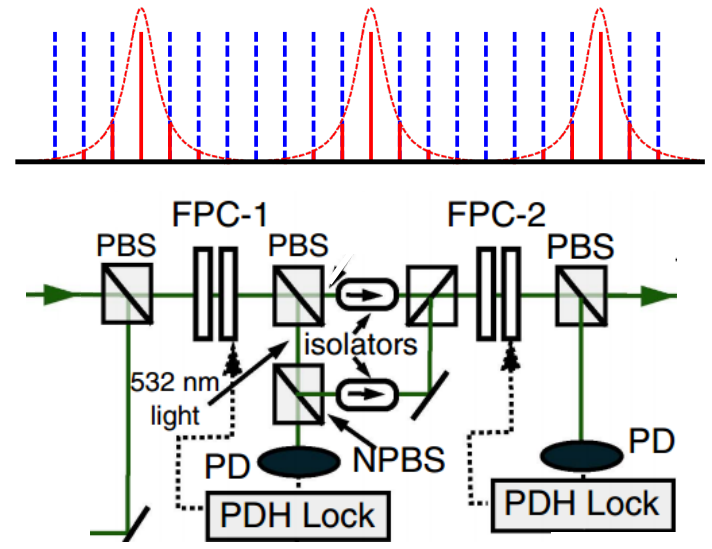
"Wobbling" parent star

Exoplanet

Star Spectrum

Astro-comb – as a wavelength reference

Astrophysical spectrograph

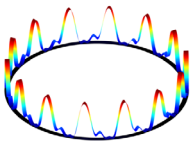


Finite side mode suppression and the instability of the external Fabry-Perot cavities are the limiting factor in precision.

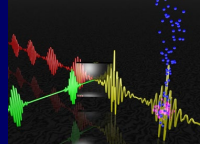
C.-H. Li *et al*, *Nature* **452**, 610 (2008).
 A. G. Glenday *et al.*, *Optica* **2**, 250 (2015).

- Year-long precision radial velocity measurements will identify habitable exoplanets
- An ideal wavelength calibrator must have thousands of calibration lines, a bandwidth of >100 nm, a comb spacing of >10 GHz, an uniform comb line power of >100 nW, and a fractional uncertainty of $<3 \times 10^{-11}$.

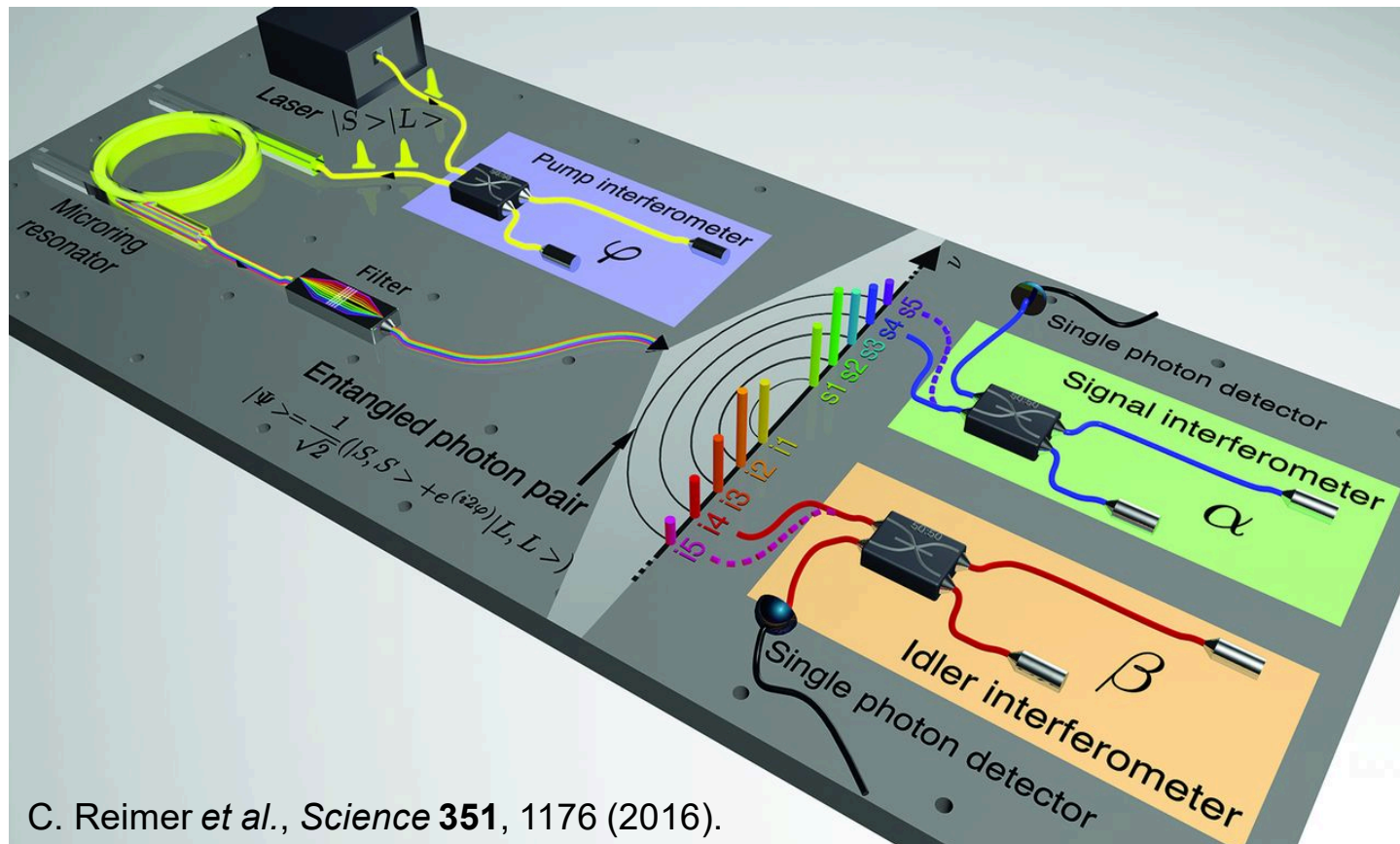




Optical quantum information processing

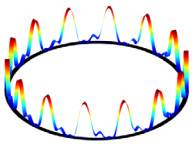


“The exploitation of integrated Kerr frequency combs, with their ability to generate multiple, customizable, and complex quantum states, can provide a scalable, practical, and compact platform for quantum technologies.”

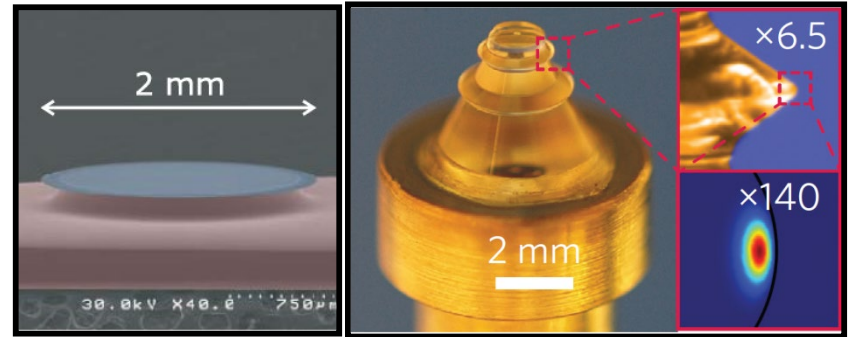
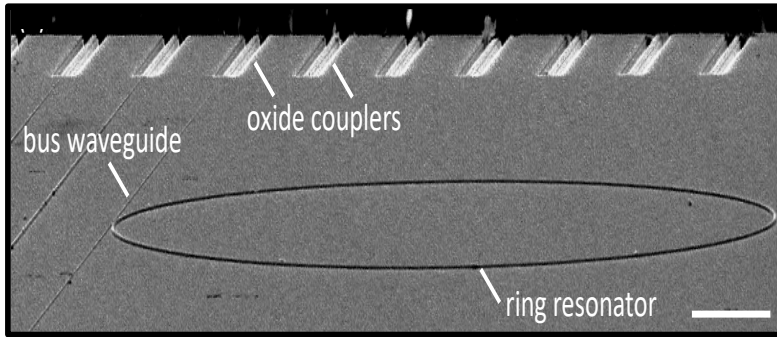
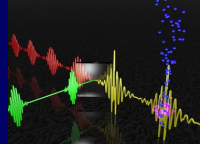


C. Reimer *et al.*, *Science* **351**, 1176 (2016).





I. Microresonator-based ultrafast light source

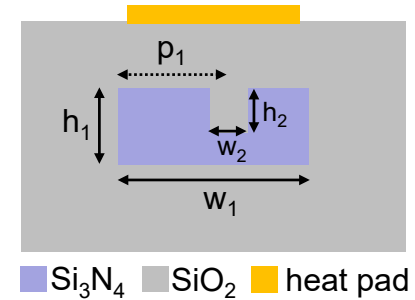
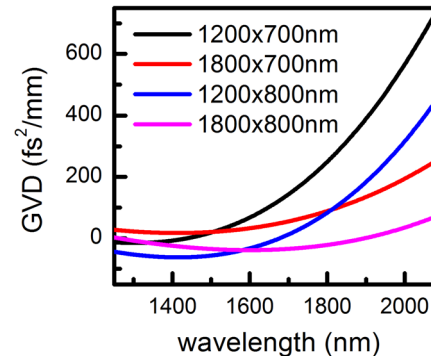


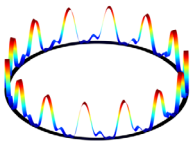
- Columbia – silicon nitride
- EPFL – silicon nitride
- Purdue – silicon nitride
- UCLA – silicon nitride**
- RMIT/INRS – Hydex
- Harvard – diamond
- Yale – aluminum nitride
- DTU – aluminum gallium arsenide

- Caltech – silica
- EPFL – CaF₂/MgF₂
- JPL – CaF₂/MgF₂
- OEwaves – CaF₂/MgF₂
- NIST – fused quartz

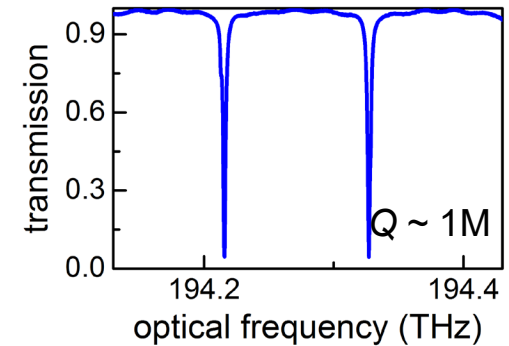
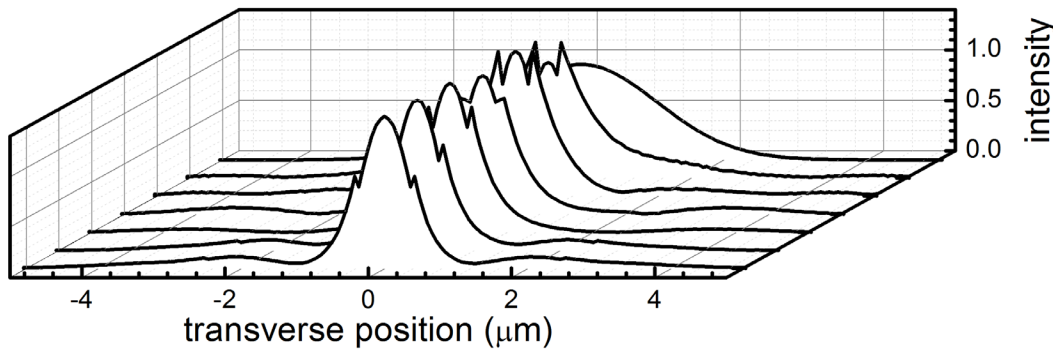
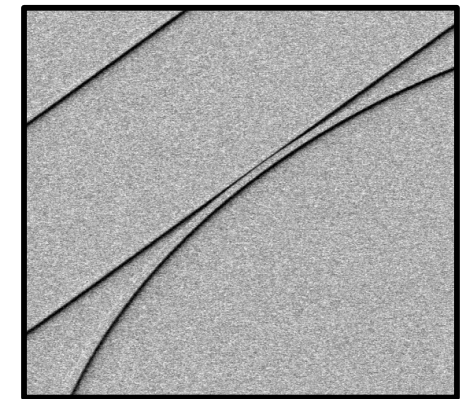
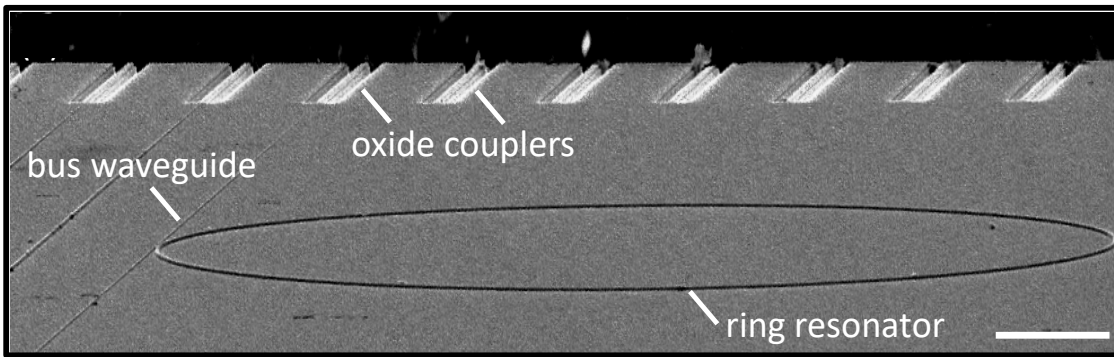
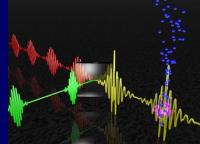
planar ring cavities are attractive

1. potential of electronic-photonic integration
2. flexibility of tailoring cavity dispersion





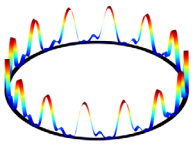
Baseline process control: Si_3N_4 μ resonators



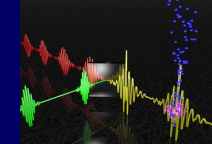
- fiber-to-fiber coupling loss is 5 dB
- smallest feature is 200 nm
- sidewall angle is 88 degree
- propagation loss is 0.2 dB/cm

fabricated in the Institute of Microelectronics Singapore



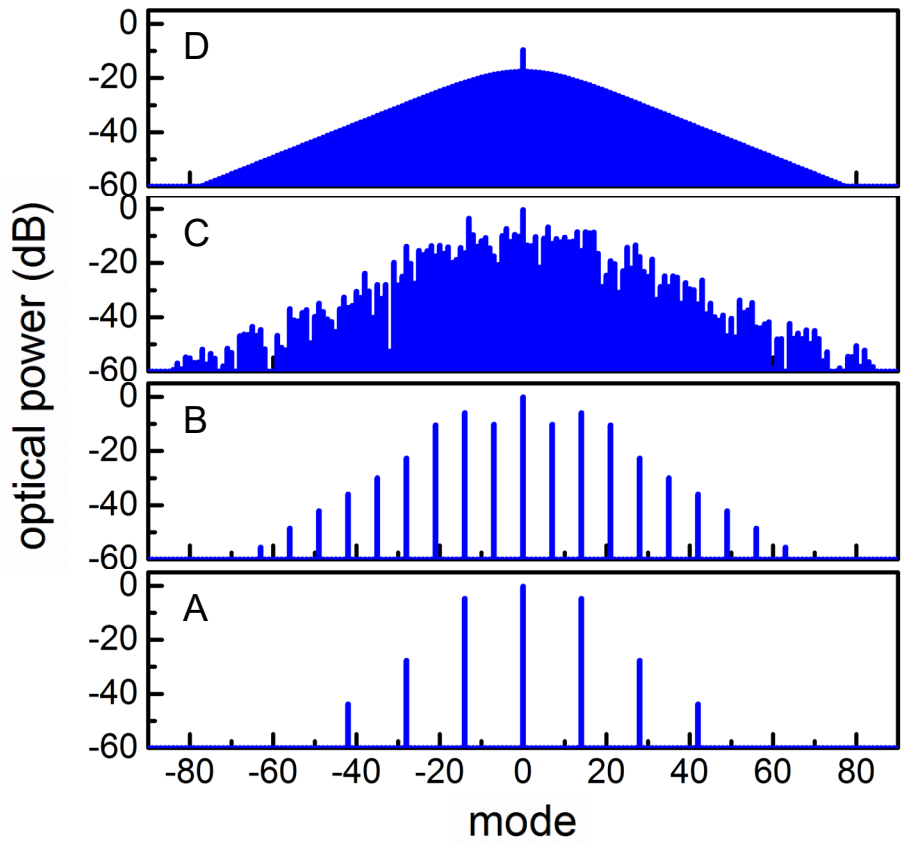
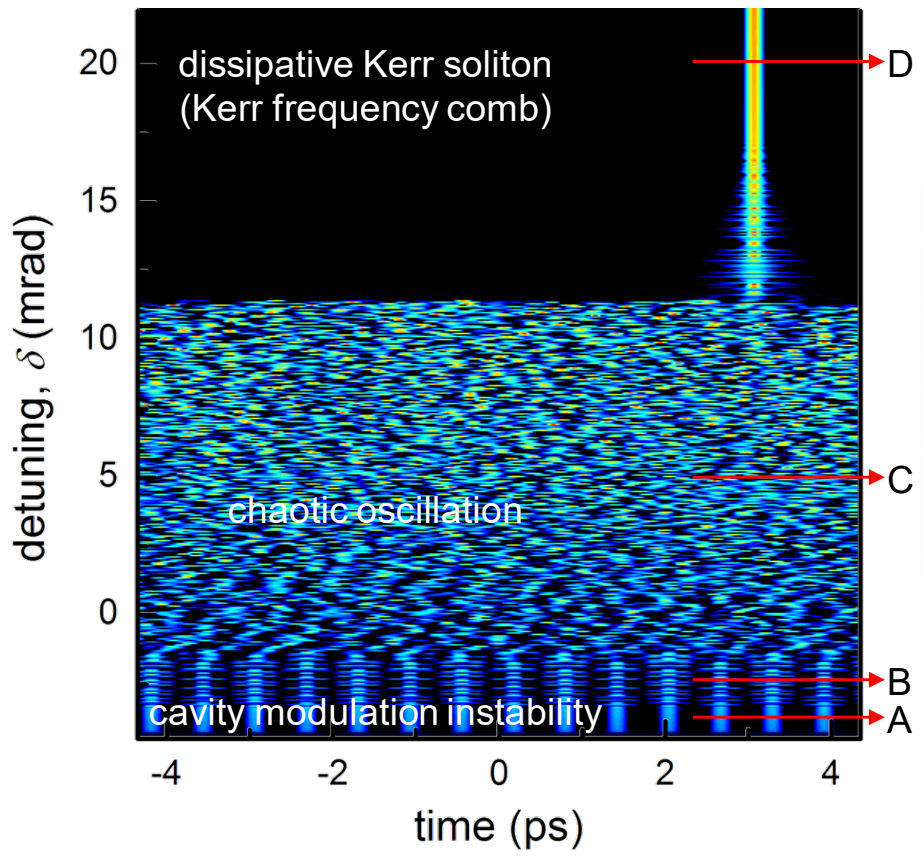


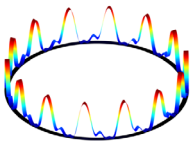
Nonlinear dynamics in microresonators



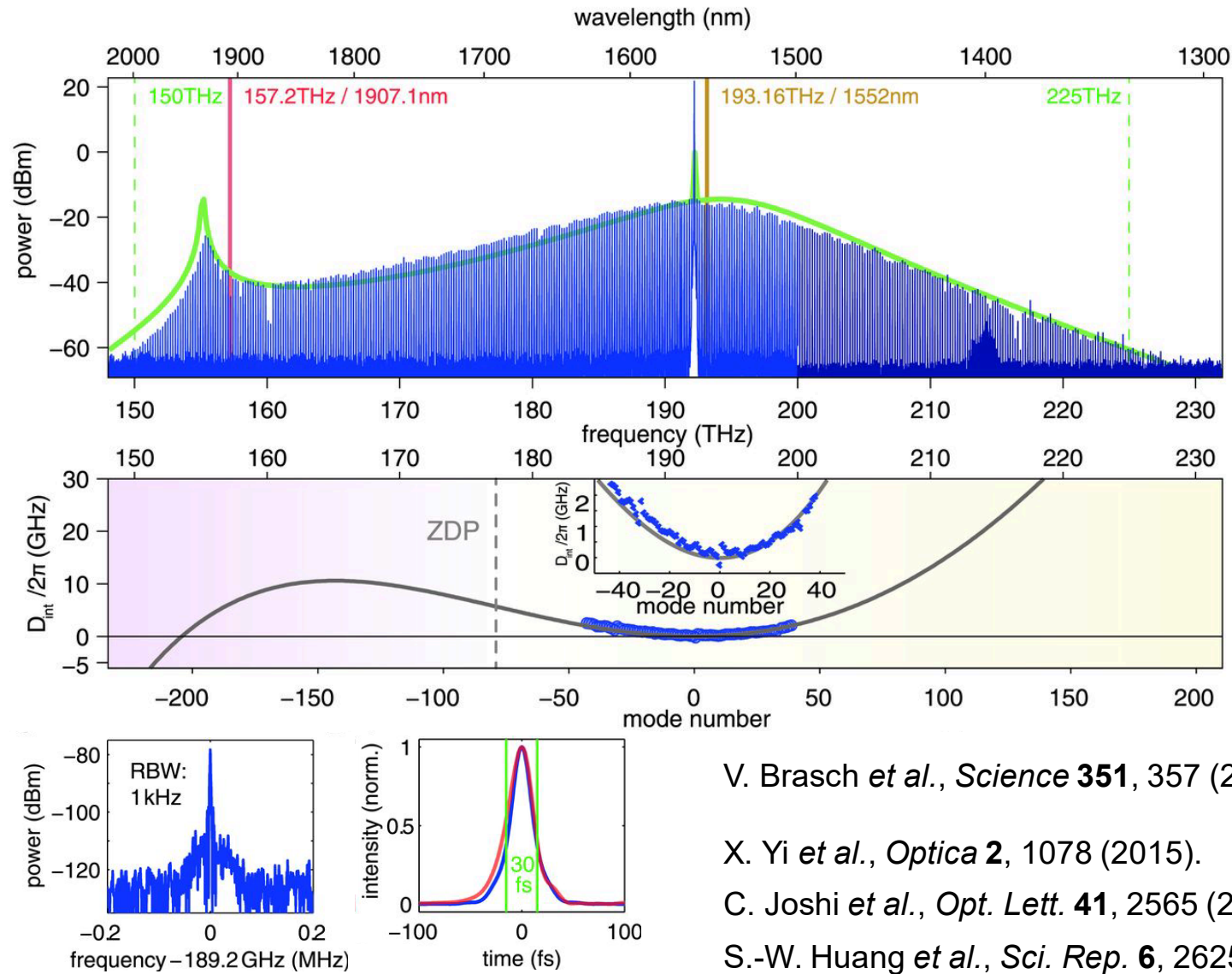
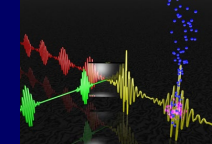
$$T_R \frac{\partial}{\partial T} A = - \left(\frac{\alpha}{2} + \frac{T}{2} + j\delta \right) A + j \frac{\beta_{2\Sigma}}{2} \frac{\partial^2}{\partial t^2} A - j\gamma_{\Sigma} |A|^2 A + \sqrt{T} A_{in}$$

detuning GVD SPM pump



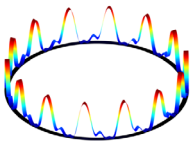


Pulses in anomalous GVD μ resonators

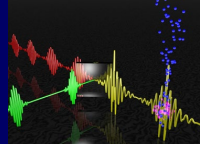


V. Brasch *et al.*, *Science* **351**, 357 (2016).
X. Yi *et al.*, *Optica* **2**, 1078 (2015).
C. Joshi *et al.*, *Opt. Lett.* **41**, 2565 (2016).
S.-W. Huang *et al.*, *Sci. Rep.* **6**, 26255 (2016).

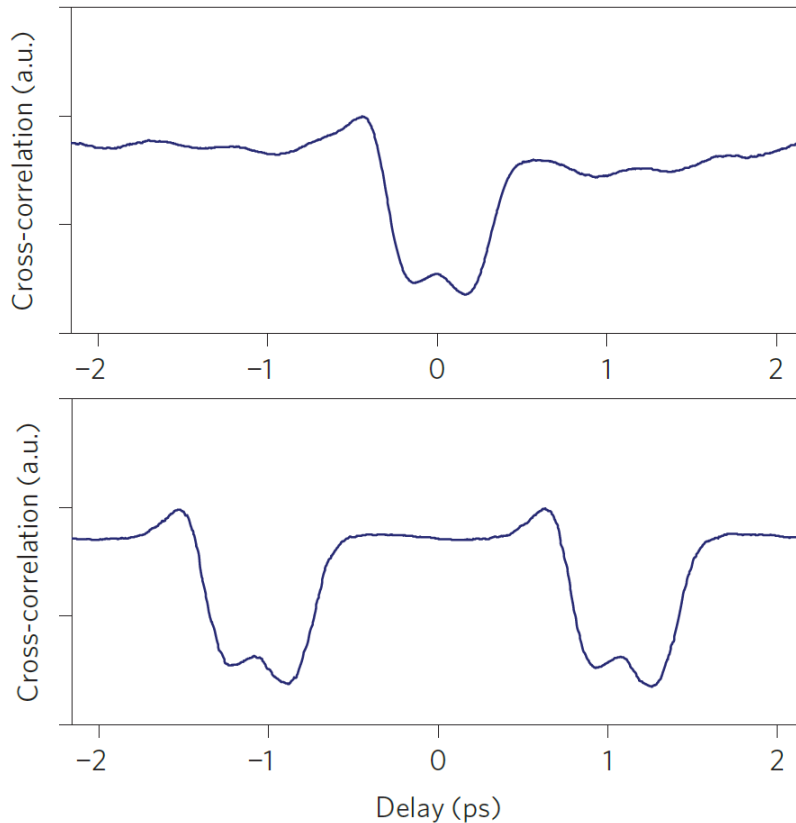




Pulses in normal GVD μ resonators

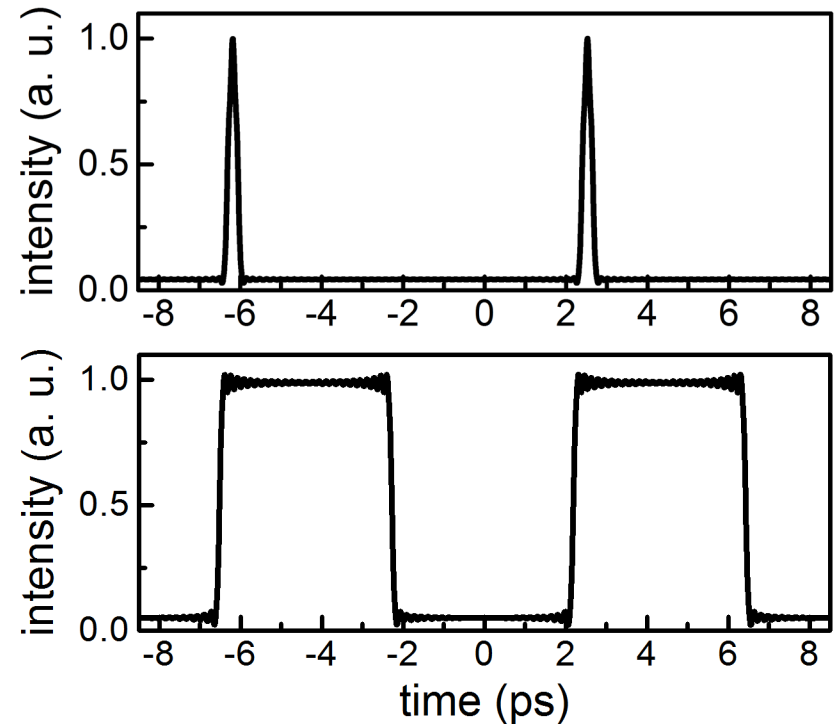


dark pulses



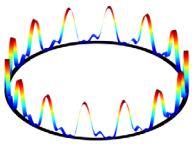
$$T_R \frac{\partial}{\partial T} A = - \left(\frac{\alpha}{2} + \frac{T}{2} + j\delta \right) A + \sqrt{T} A_{in} \\ + j \left(\frac{\beta_{2\Sigma}}{2} - j \frac{T}{\Omega_f^2} \right) \frac{\partial^2}{\partial t^2} A - j\gamma_\Sigma |A|^2 A$$

intracavity filtering

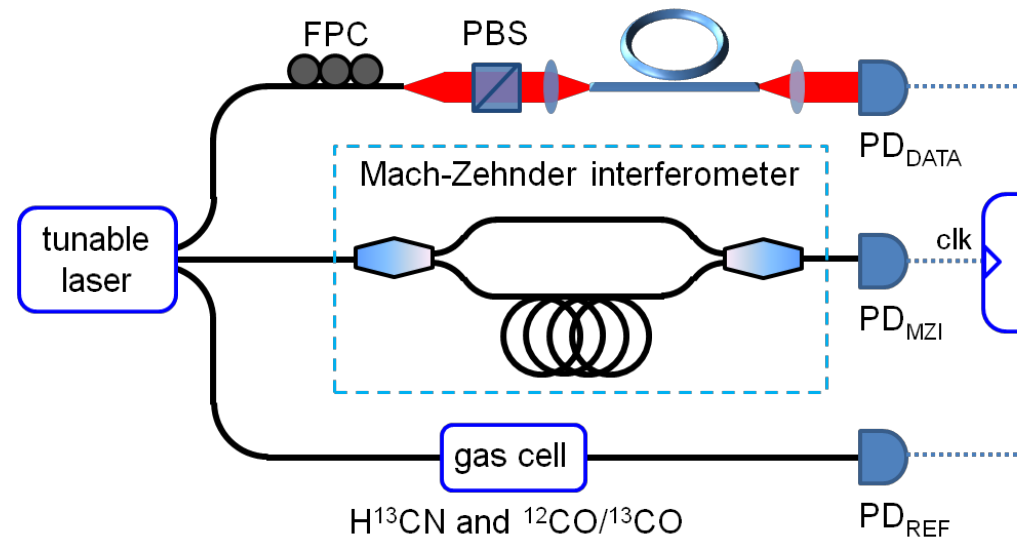
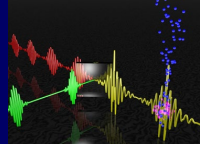


X. Xue *et al.*, *Nat. Photon.* **9**, 594 (2015).

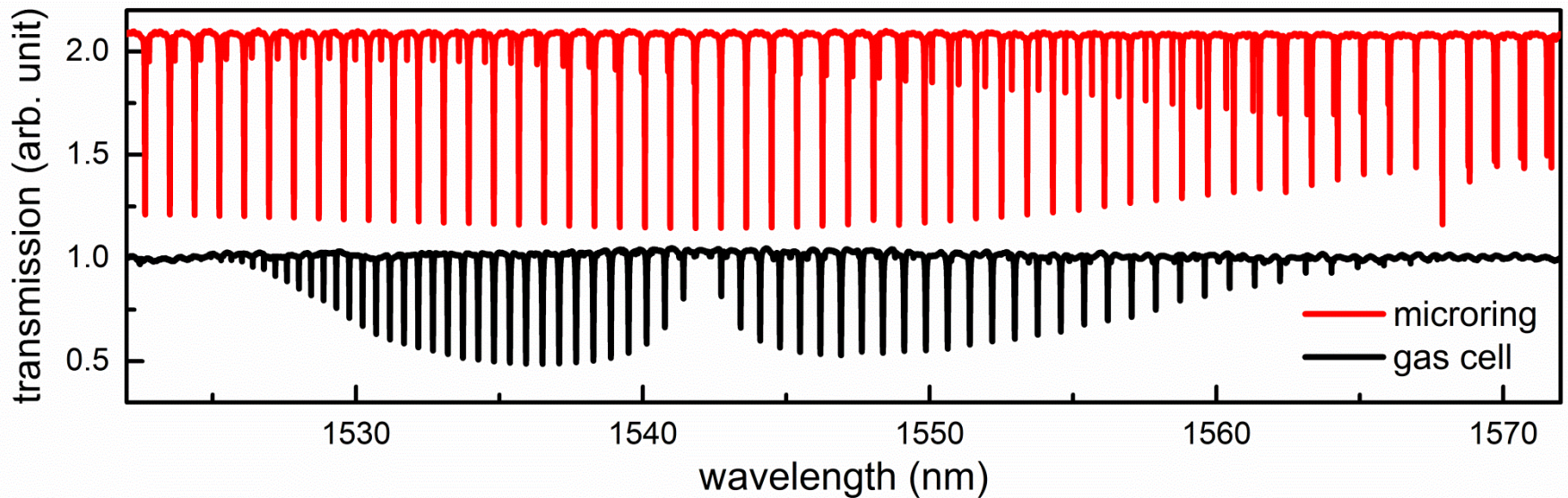


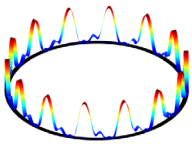


Coherent swept wavelength interferometer

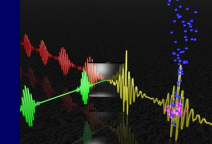


- scan speed: >40 nm/s
- MZI clock: 5 MHz sampling
- synchronous gas cell measurement
- active temperature stabilization

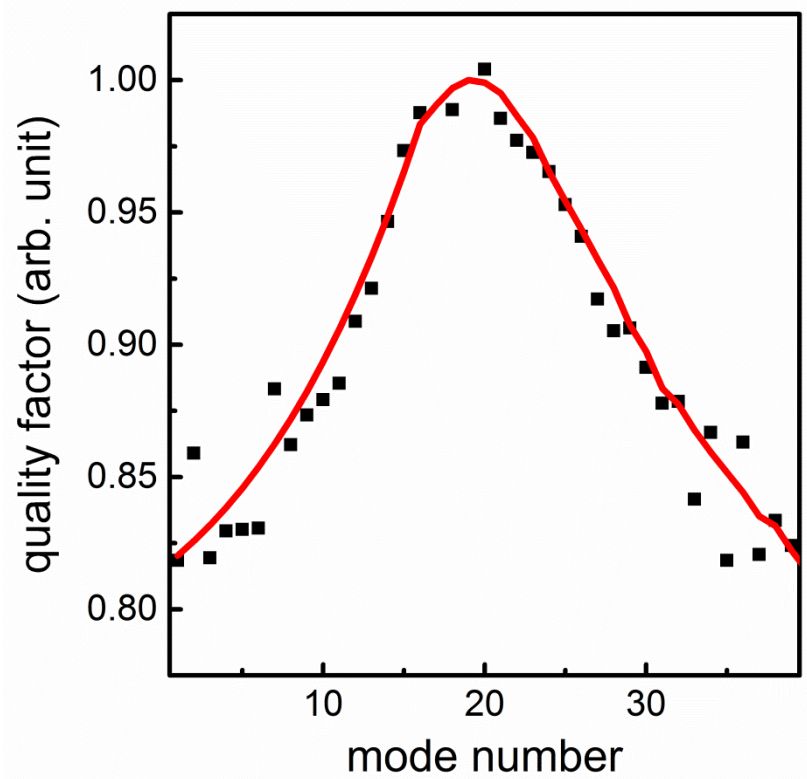
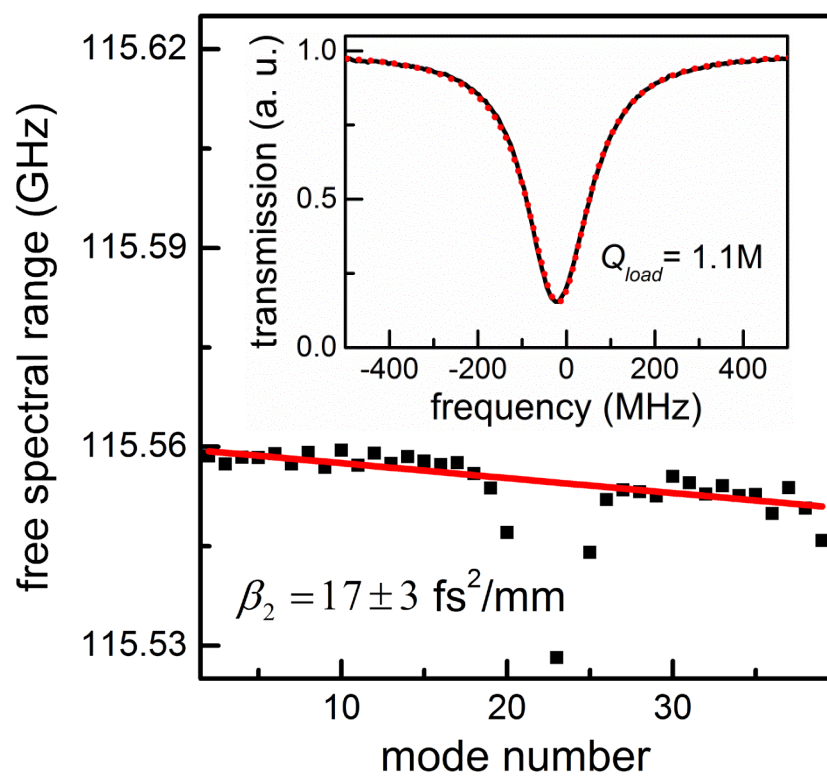


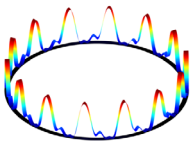


Measurements of GVD and intracavity filter

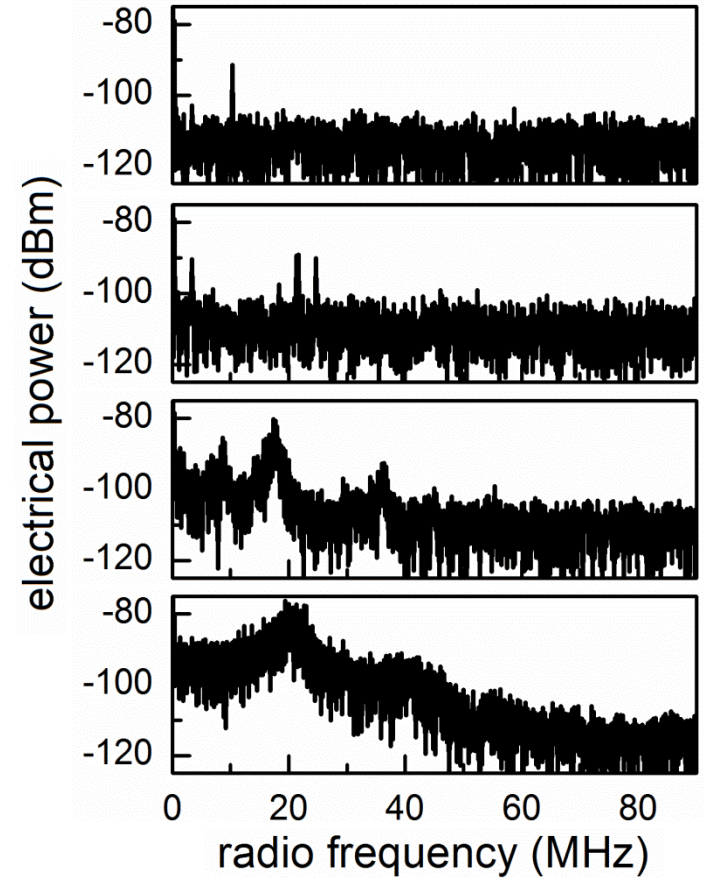
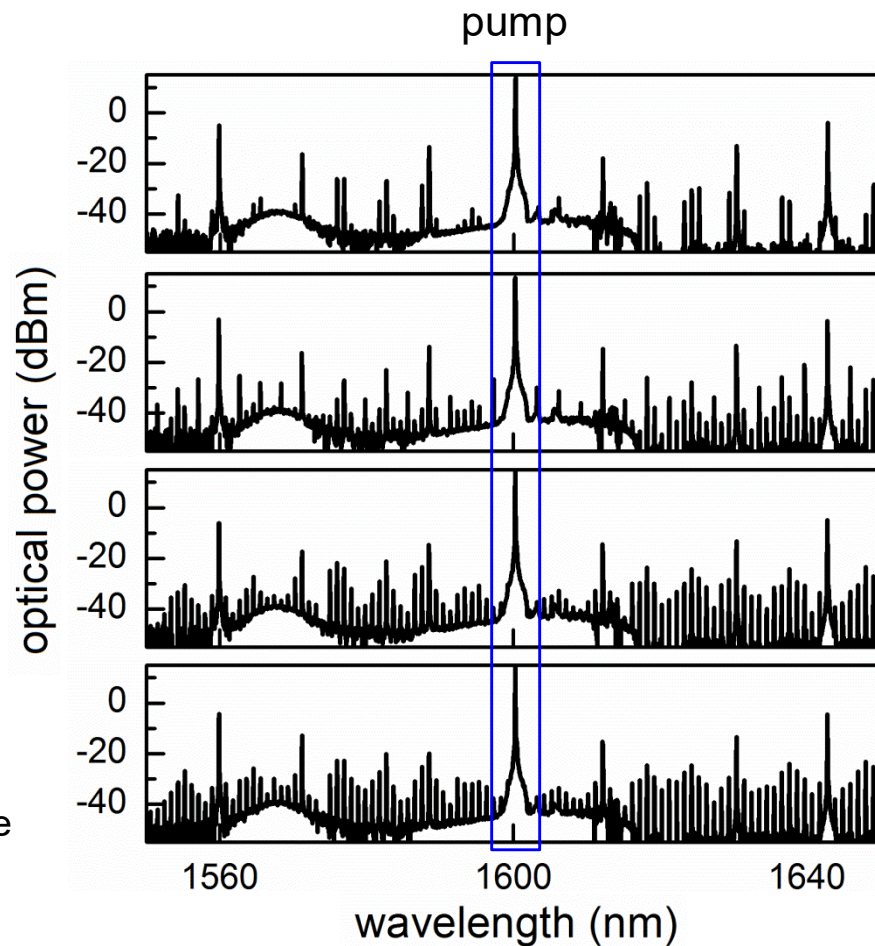
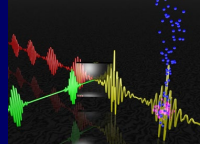


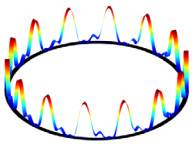
Each resonance is fitted with a Lorentzian lineshape to find the resonance frequency and the quality factor. The GVD is then determined by analyzing the dependence of the free spectral range on the mode number.



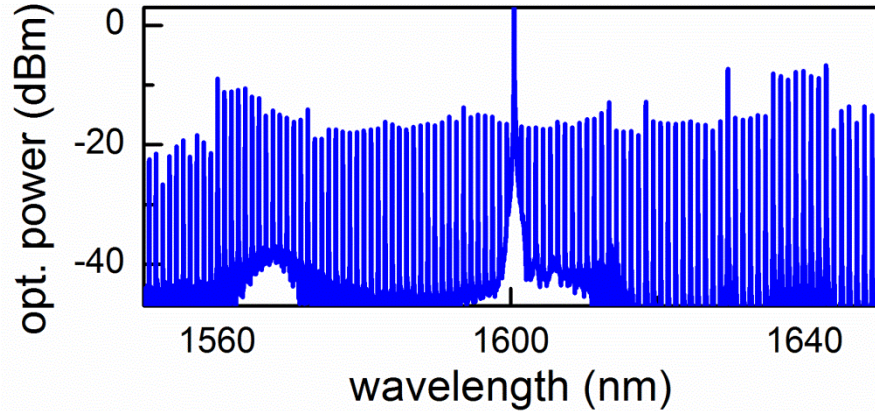
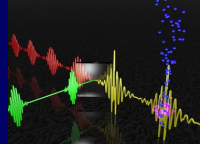


State evolution in microresonator

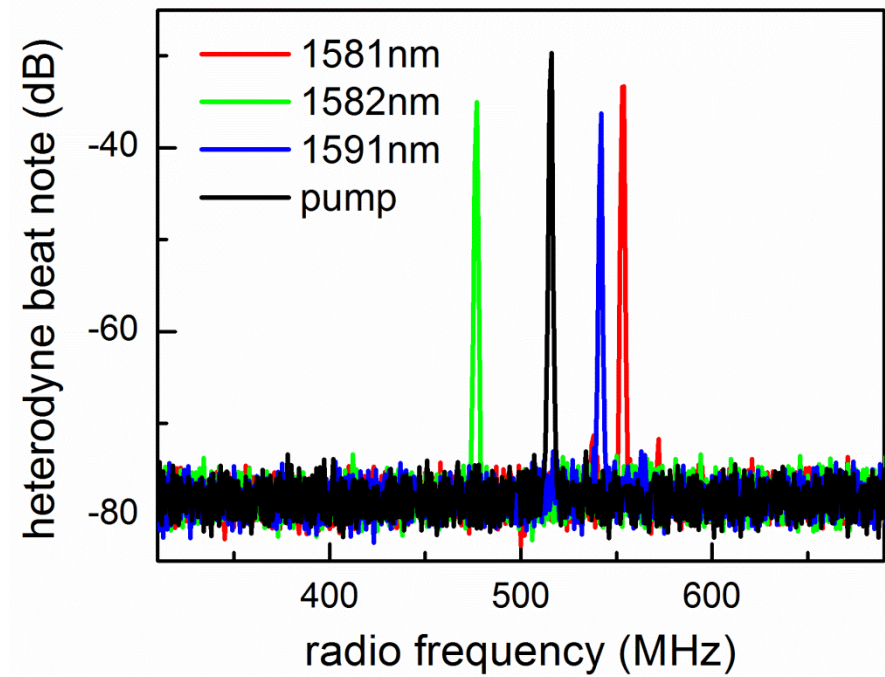
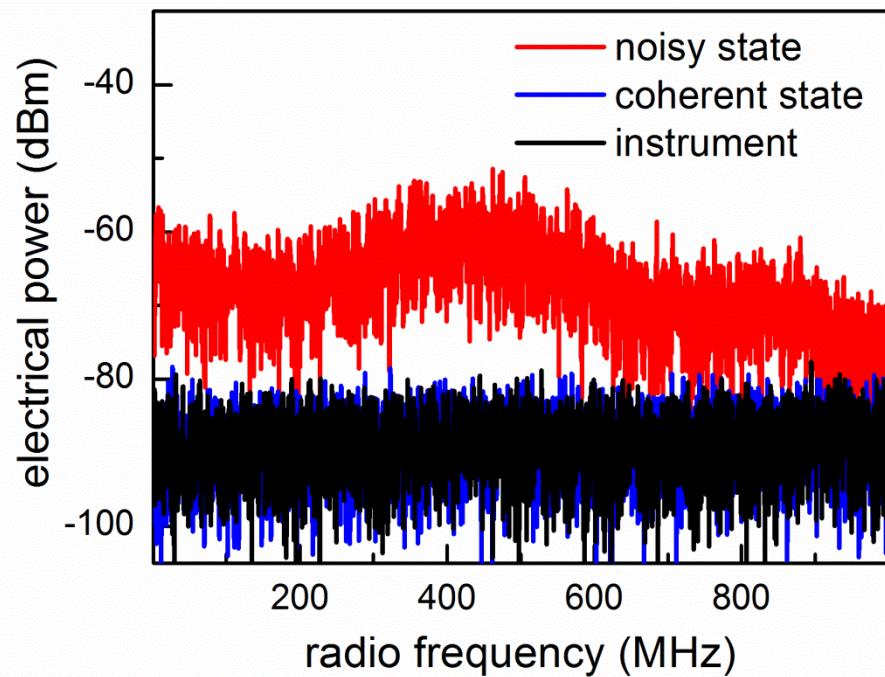


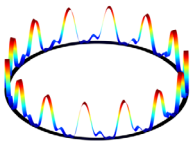


Establishment of coherence

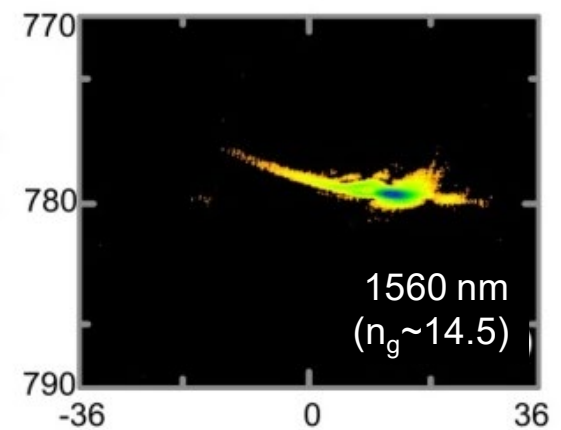
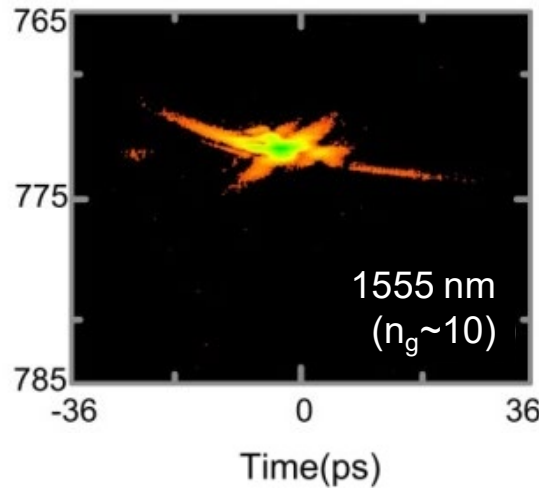
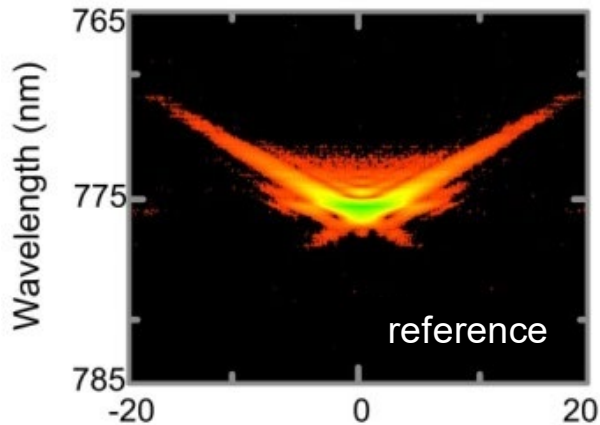
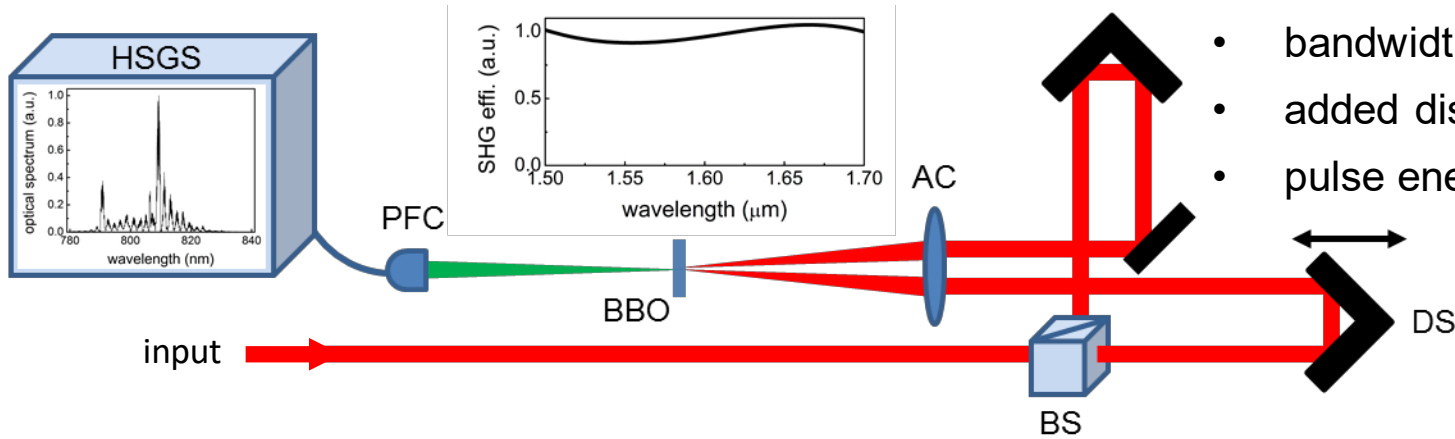
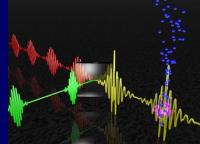


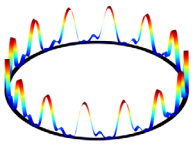
- A stepwise change of resonance detuning or pump power drives the microresonator into the Kerr frequency comb state.
- All heterodyne beat notes exhibit the same linewidth of 800 kHz, limited by the mutual coherence of the pump and the reference.



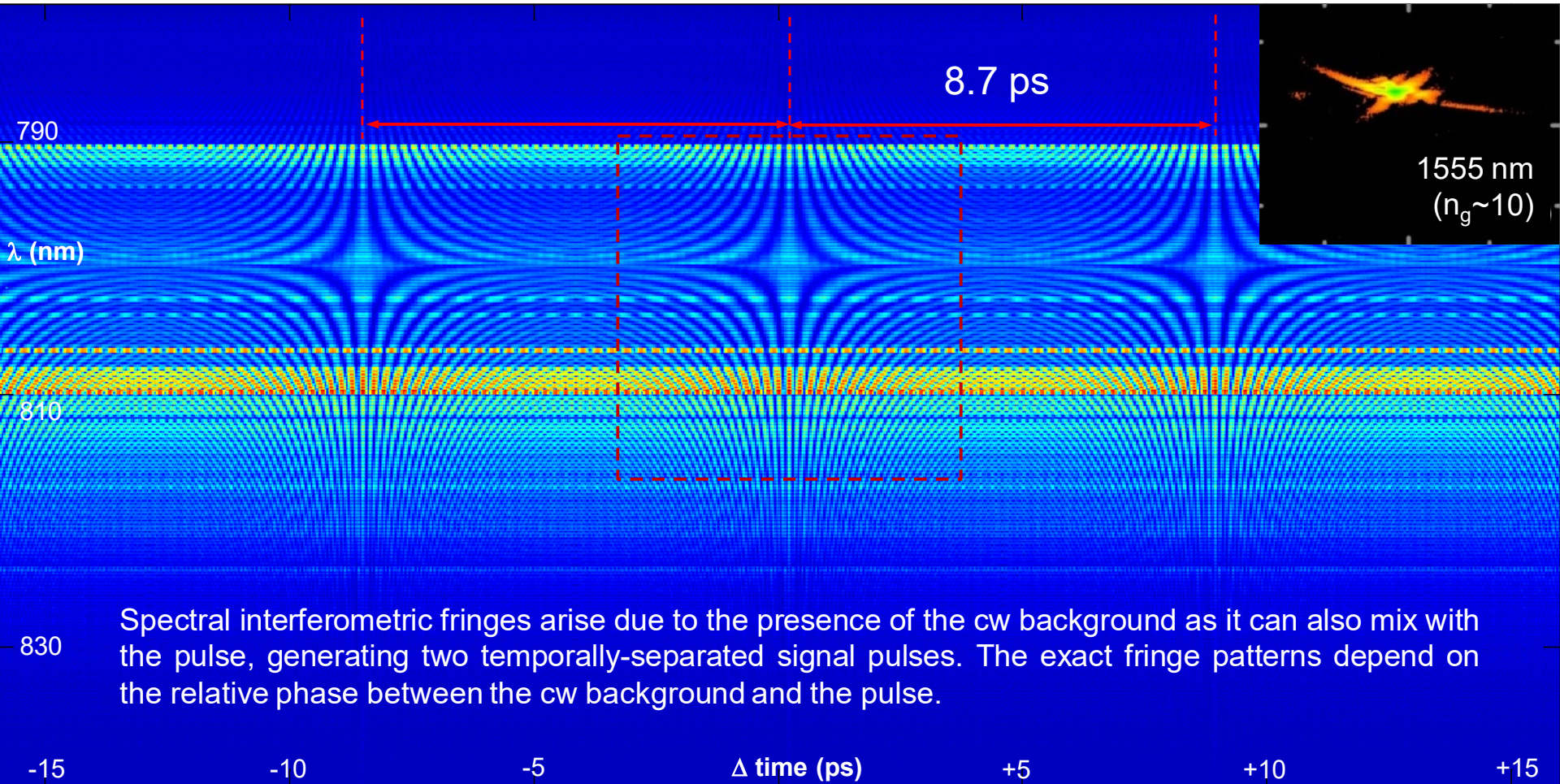
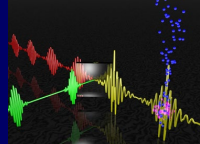


Frequency resolved optical gating (FROG)



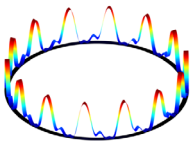


FROG spectrogram

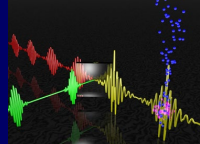


Spectral interferometric fringes arise due to the presence of the cw background as it can also mix with the pulse, generating two temporally-separated signal pulses. The exact fringe patterns depend on the relative phase between the cw background and the pulse.

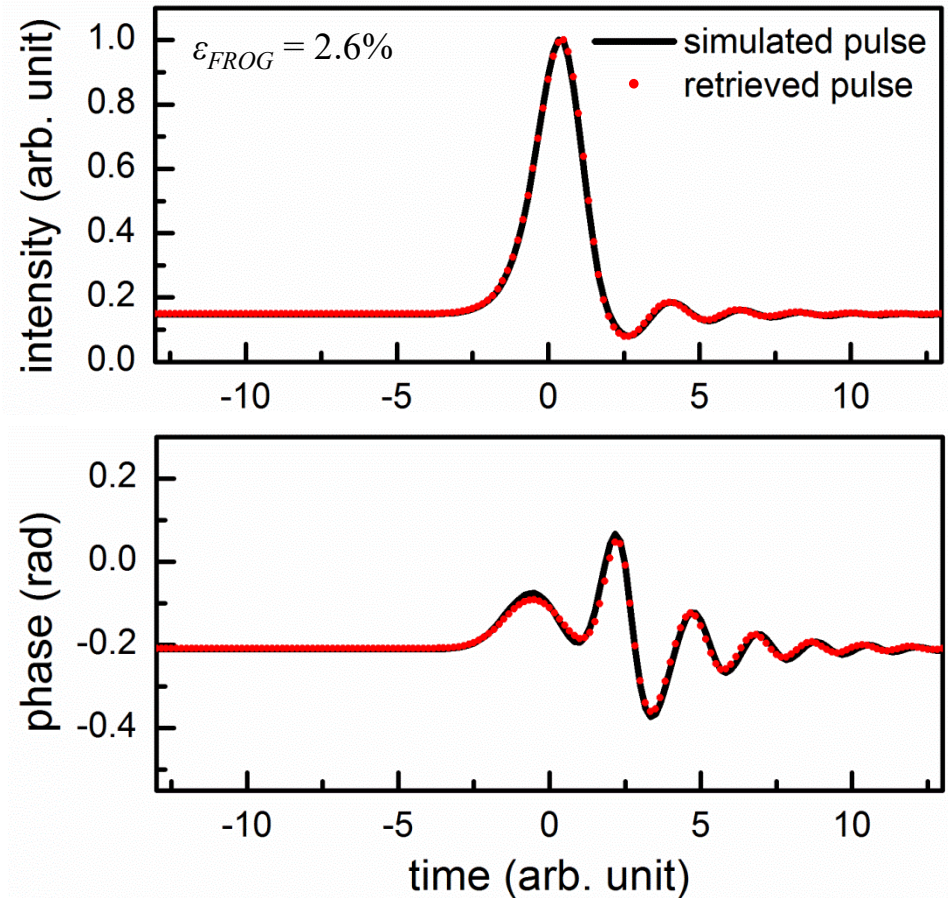
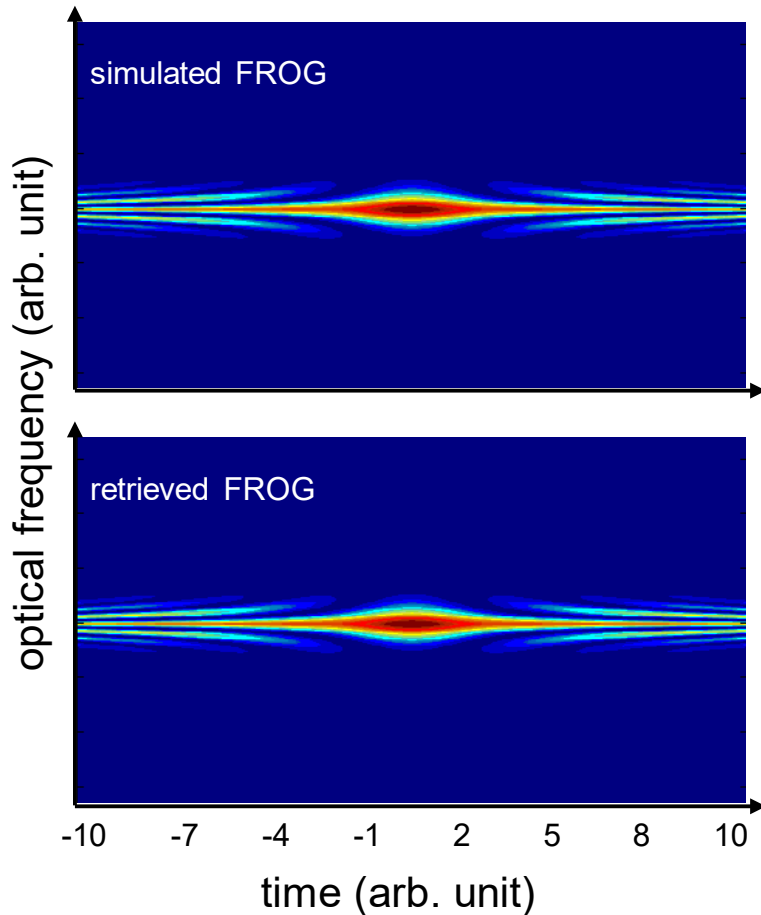


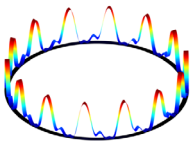


Genetic algorithm for phase retrieval

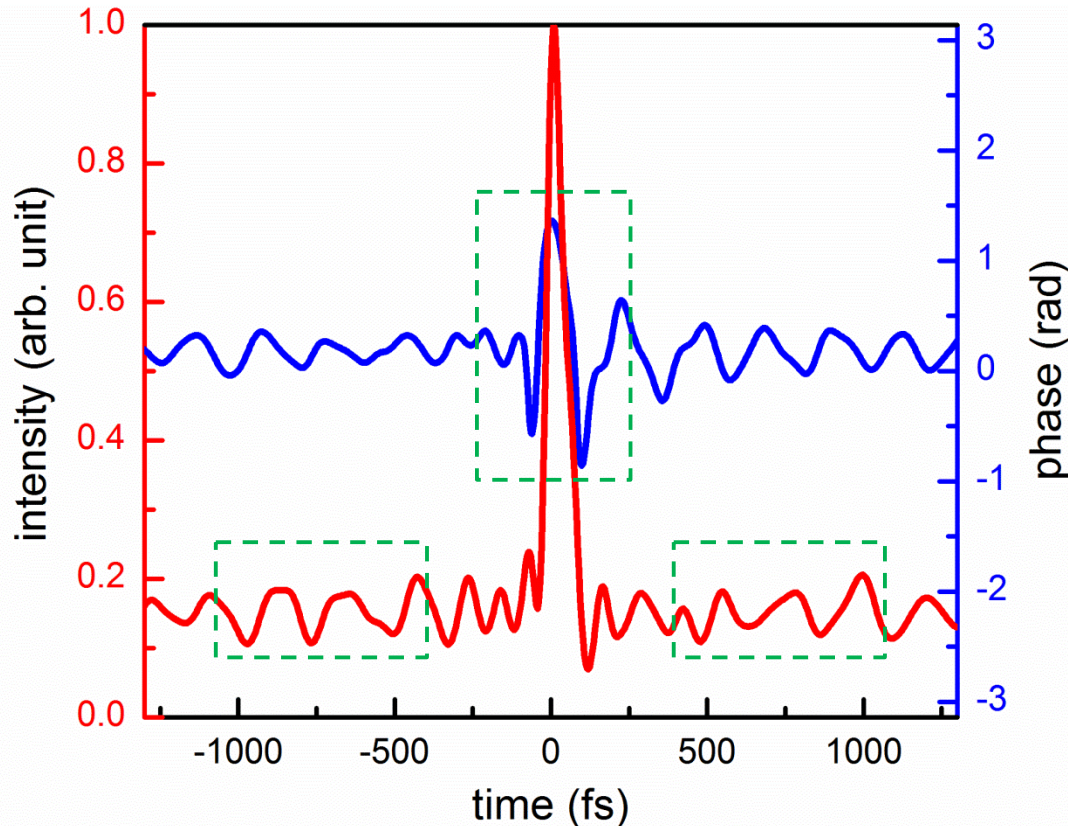
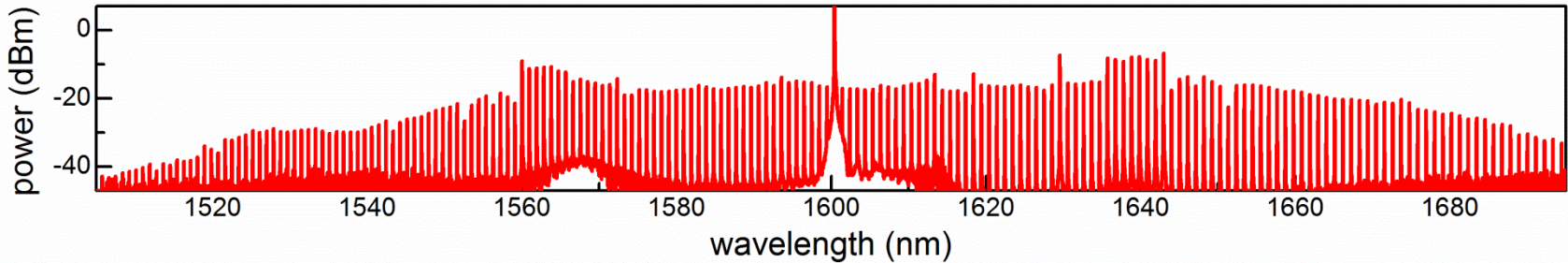
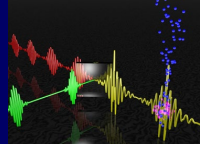


Genetic algorithm is a global search method based on ideas taken from evolution and is less susceptible to becoming trapped by local extrema in the search space.





FROG retrieved pulse structure

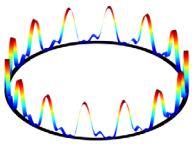


pulse duration is 74 fs,
positively chirped from the
ideal pulse duration of 55 fs

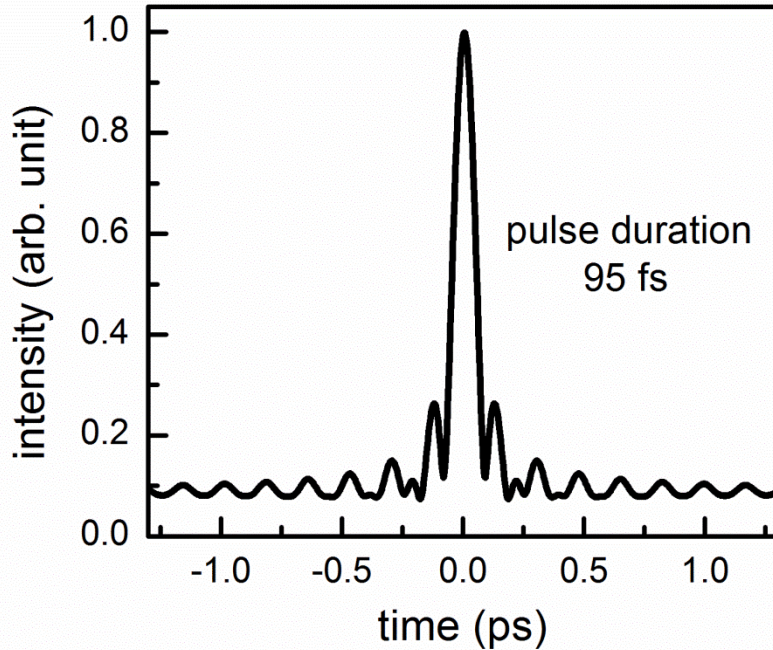
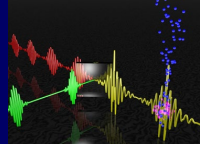
1.3 rad phase contrast is
observed within the pulse

continuous-wave background
is essential for the existence
of stable pulses





Bright pulse and analytic solution



pulse peak power is much higher than cw background

$$|A_{p0}|^2 / |A_c|^2 \gg 1$$

pulse energy is much lower than cw energy

$$\int_0^{T_R} |A_c|^2 dt / \int_0^{T_R} |A_p|^2 dt \gg 1$$

time bandwidth product is much larger than unity

$$q^2 \gg \Omega_f^2 \tau^2 \gg 1$$

ansatz:

$$A(T, t) = A_c + A_p(T, t)$$

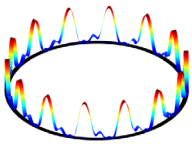
$$A_p(T, t) = A_{p0} \left[\exp\left(\frac{t}{\sqrt{2}\tau}\right)^2 \right]^{-1-iq} e^{i\varphi_p}$$

solution:

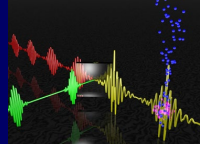
$$q \cong \frac{4\beta_{2\Sigma}\Omega_f^2}{3T} \quad \text{chirp}$$

$$\tau \cong \frac{1.5\beta_{2\Sigma}^{\frac{3}{2}}\Omega_f^2}{T\sqrt{\delta}} \quad \text{pulse duration}$$



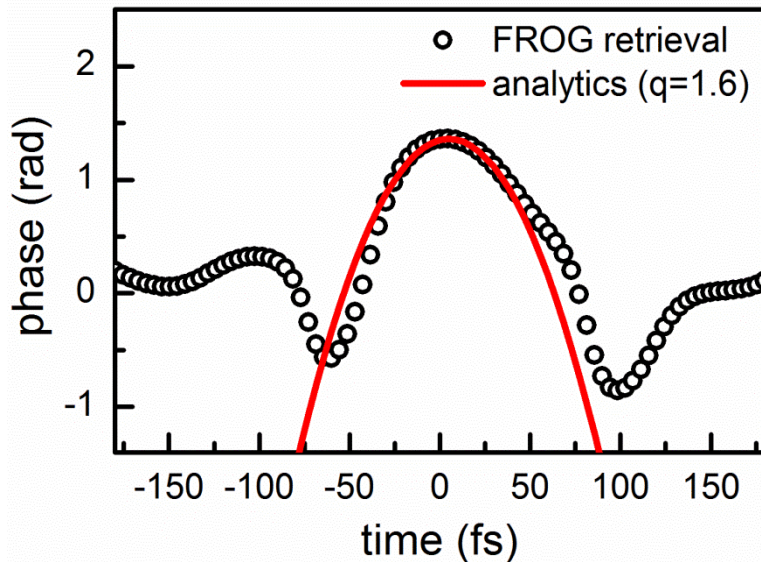


Matching with the FROG retrieval



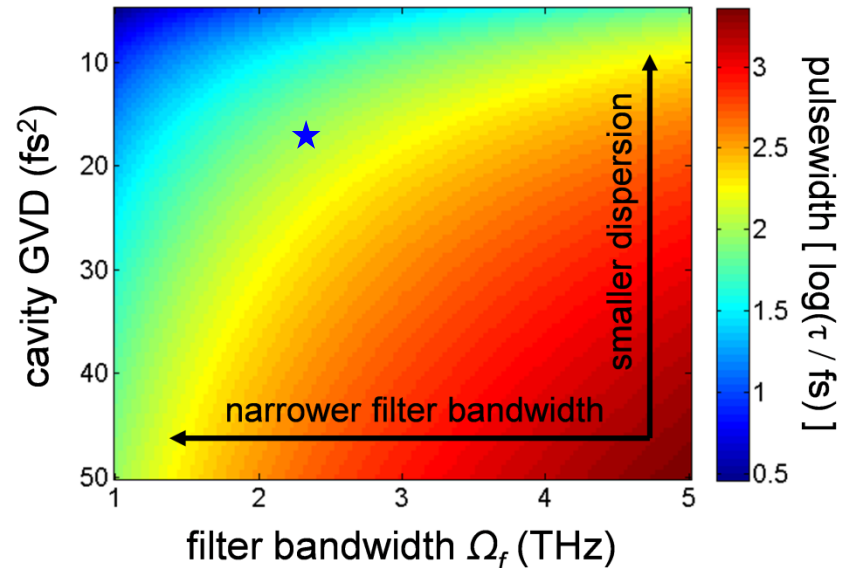
Analytically calculated chirp agrees well with the FROG retrieval.

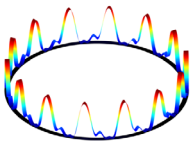
$$q \cong \frac{4\beta_{2\Sigma}\Omega_f^2}{3T}$$



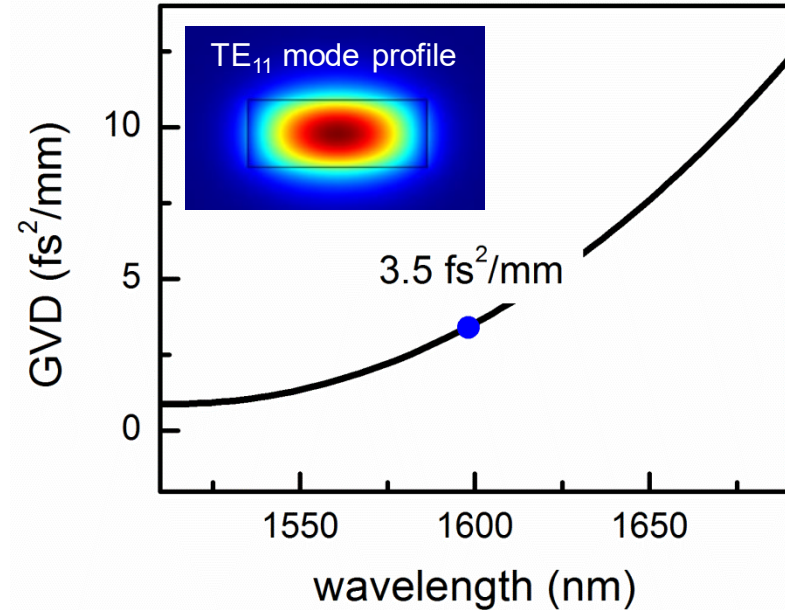
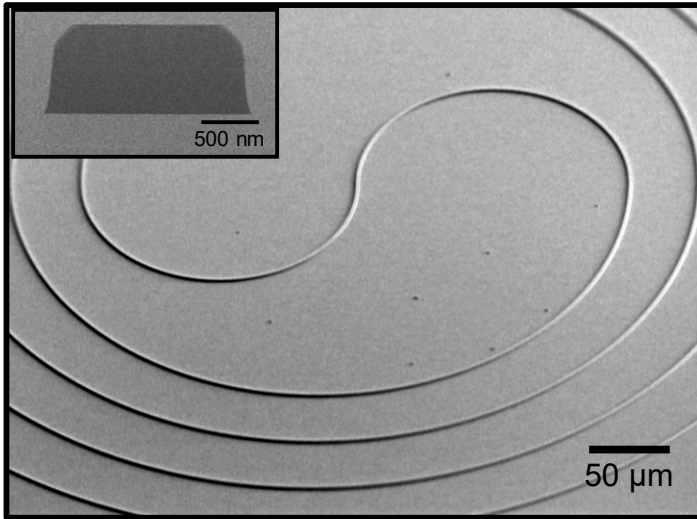
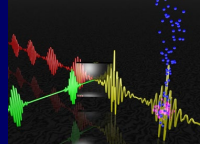
A narrower filter bandwidth and smaller GVD are beneficial for short pulses.

$$\tau \cong \frac{1.5\beta_{2\Sigma}^{\frac{3}{2}}\Omega_f^2}{T\sqrt{\delta}}$$



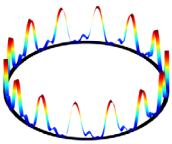


II. Low noise broadband microcomb

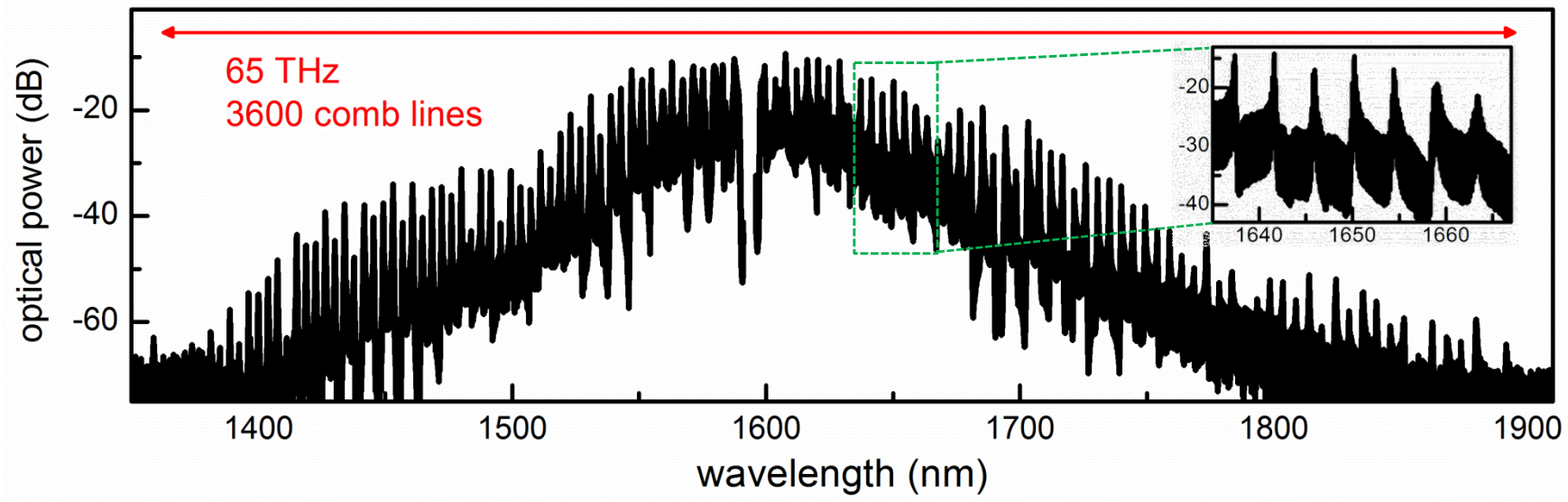
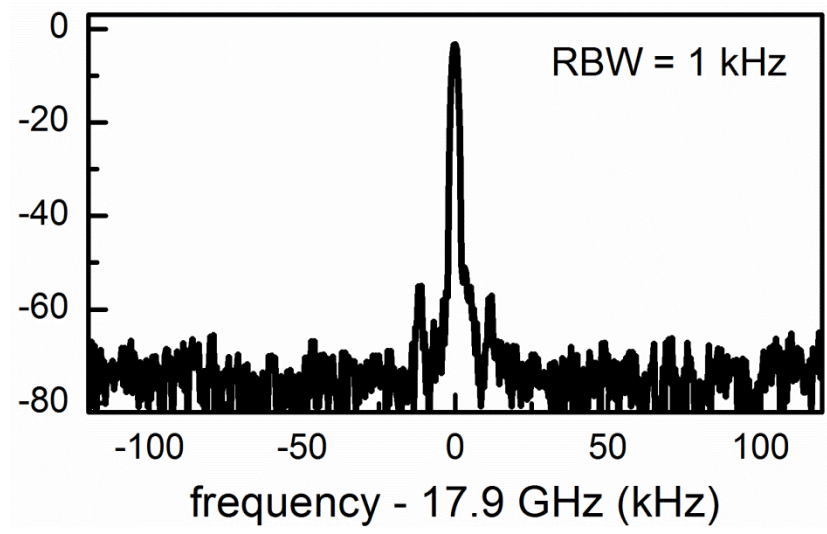
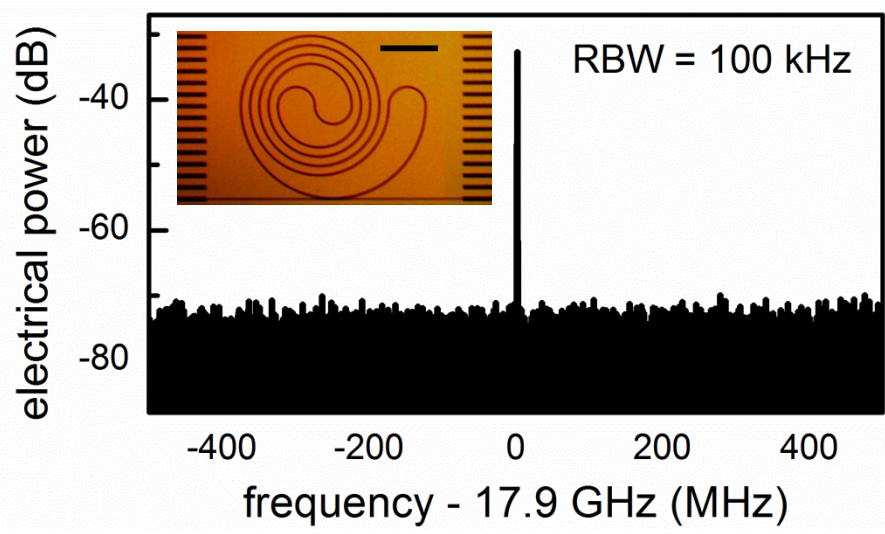
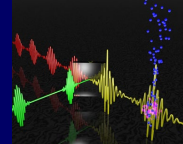


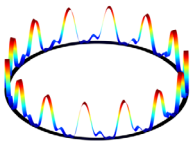
1. Microresonator-based ultrafast light source delivering 74 femtosecond pulse train
- Huang *et al.*, *Phys. Rev. Lett.* **114**, 053901 (2015).
2. Low noise broadband microcomb containing 3,600 coherent frequency teeth
- Huang *et al.*, *Sci. Rep.* **5**, 13355 (2015).
3. High bandwidth comb stabilization achieving a fractional uncertainty of 2.7×10^{-16}
- Huang *et al.*, *Sci. Adv.* **2**, e1501489 (2016).
4. Microresonator stabilized diode laser at the thermodynamical limit of 1.7×10^{-13}
- Lim *et al.*, *Opt. Lett.* **41**, 3706 (2016).



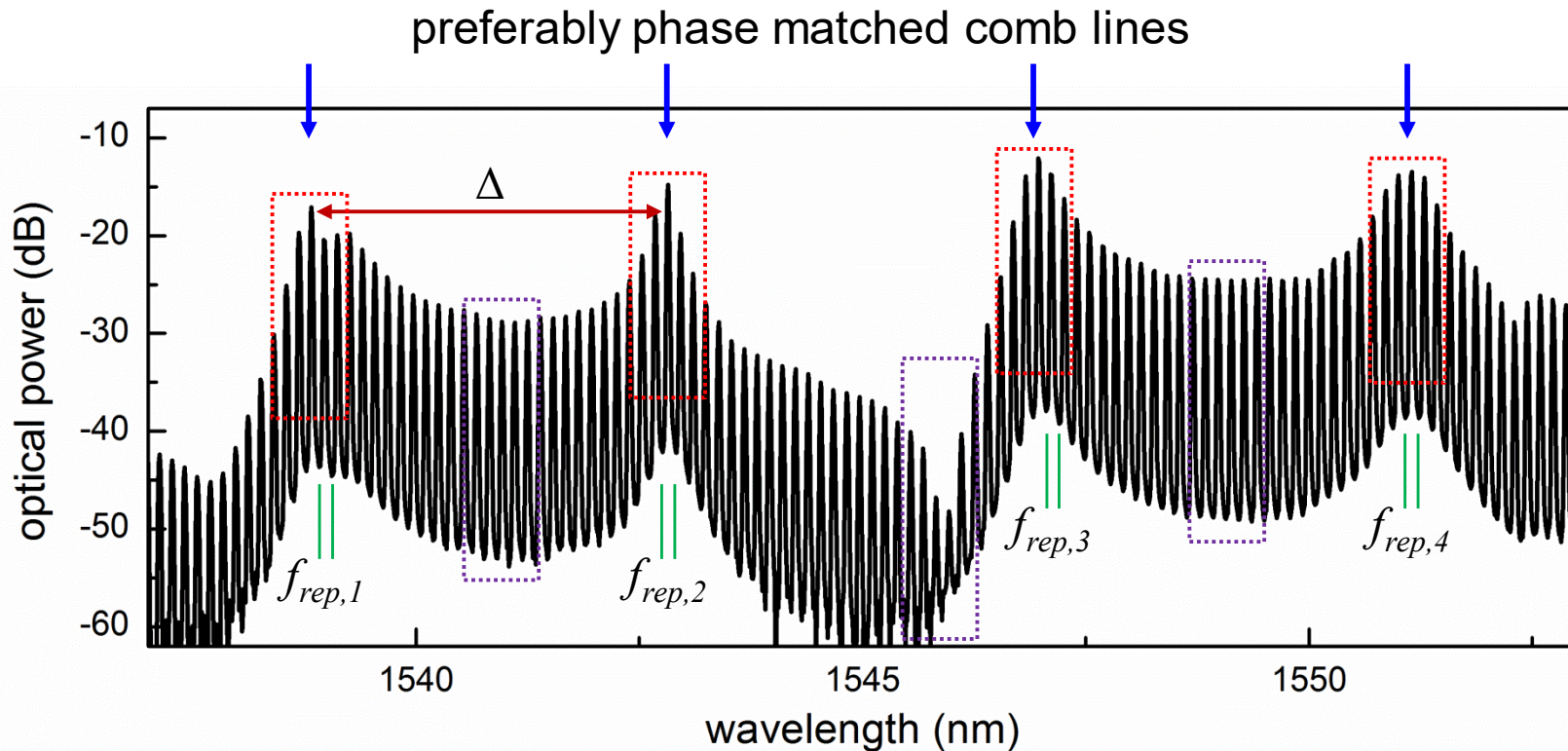
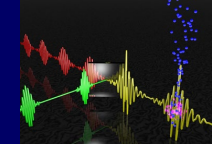


Half-octave-spanning coherent comb spectrum





Coherence between different comb families

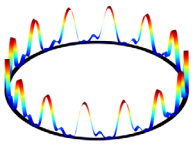


To use the constitutive equation

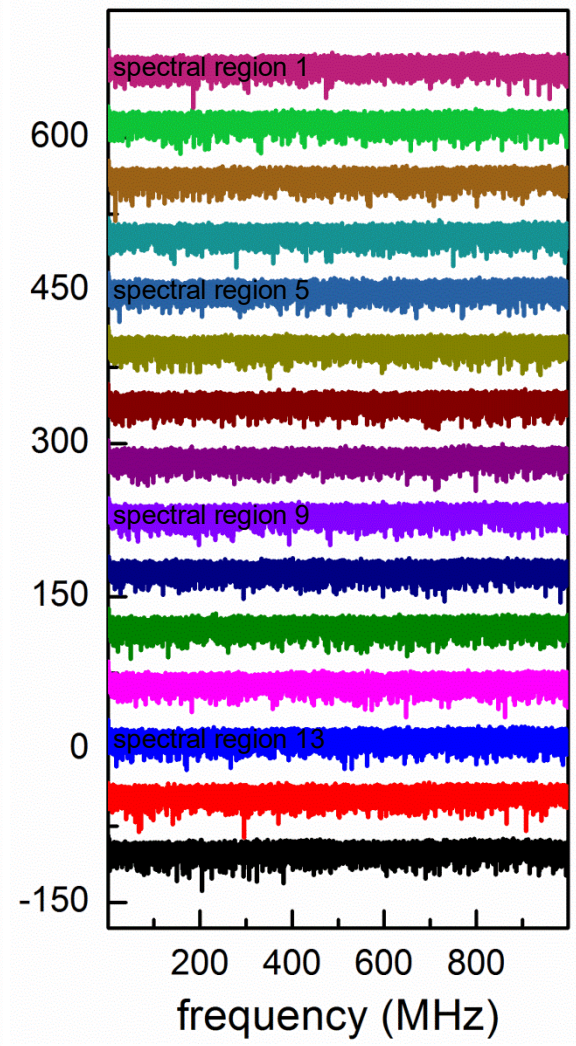
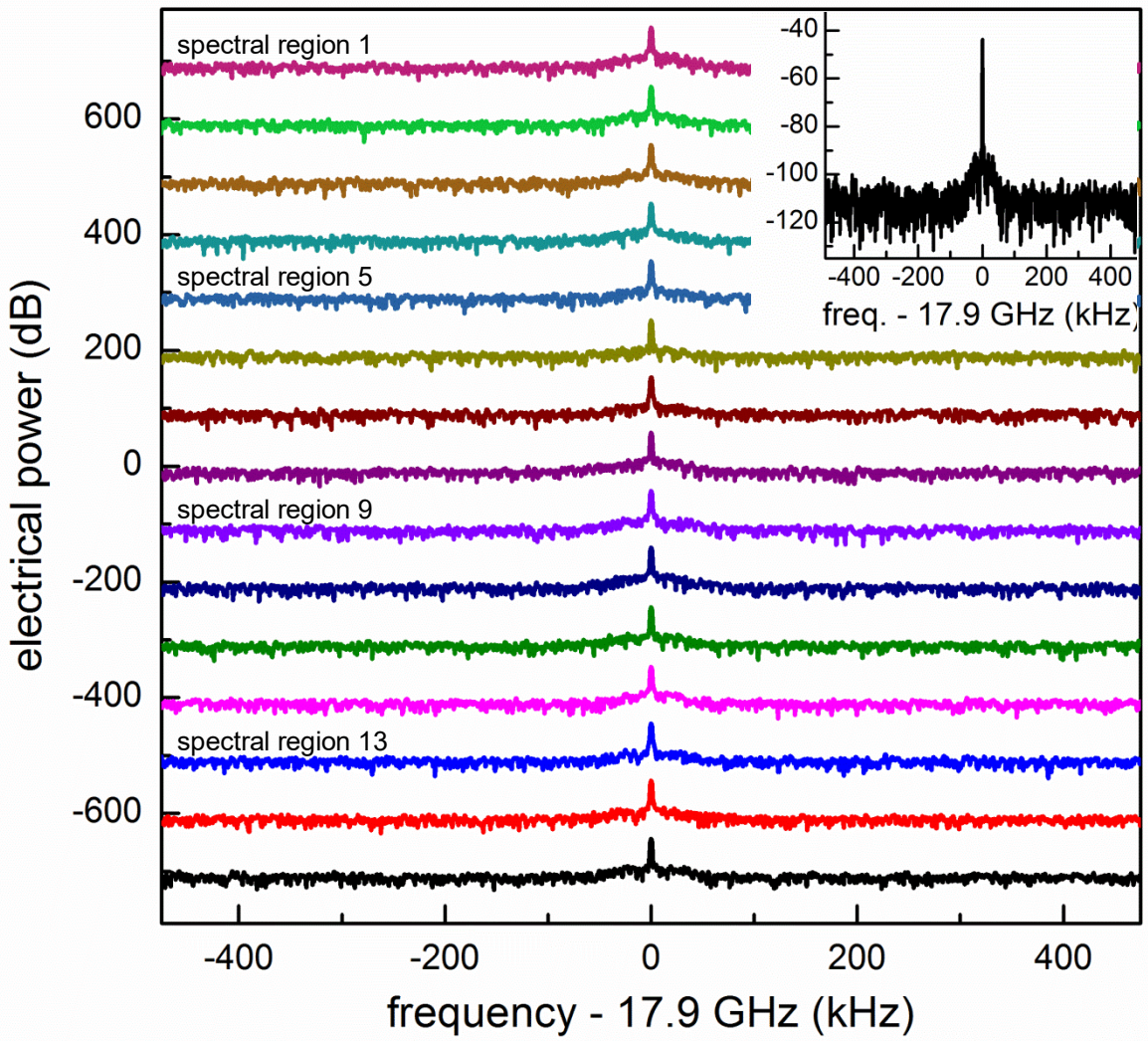
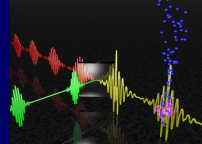
$$f_n = n \cdot f_{rep} + f_{ceo}$$

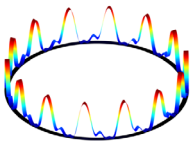
, comb spacing needs to be equal across the full spectrum $f_{rep,1} = f_{rep,2} = \dots = f_{rep}$
, and Δ needs to be commensurate with the comb spacing $\Delta = N f_{rep}$



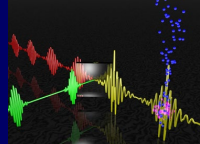


Verification of continuously-equidistant comb

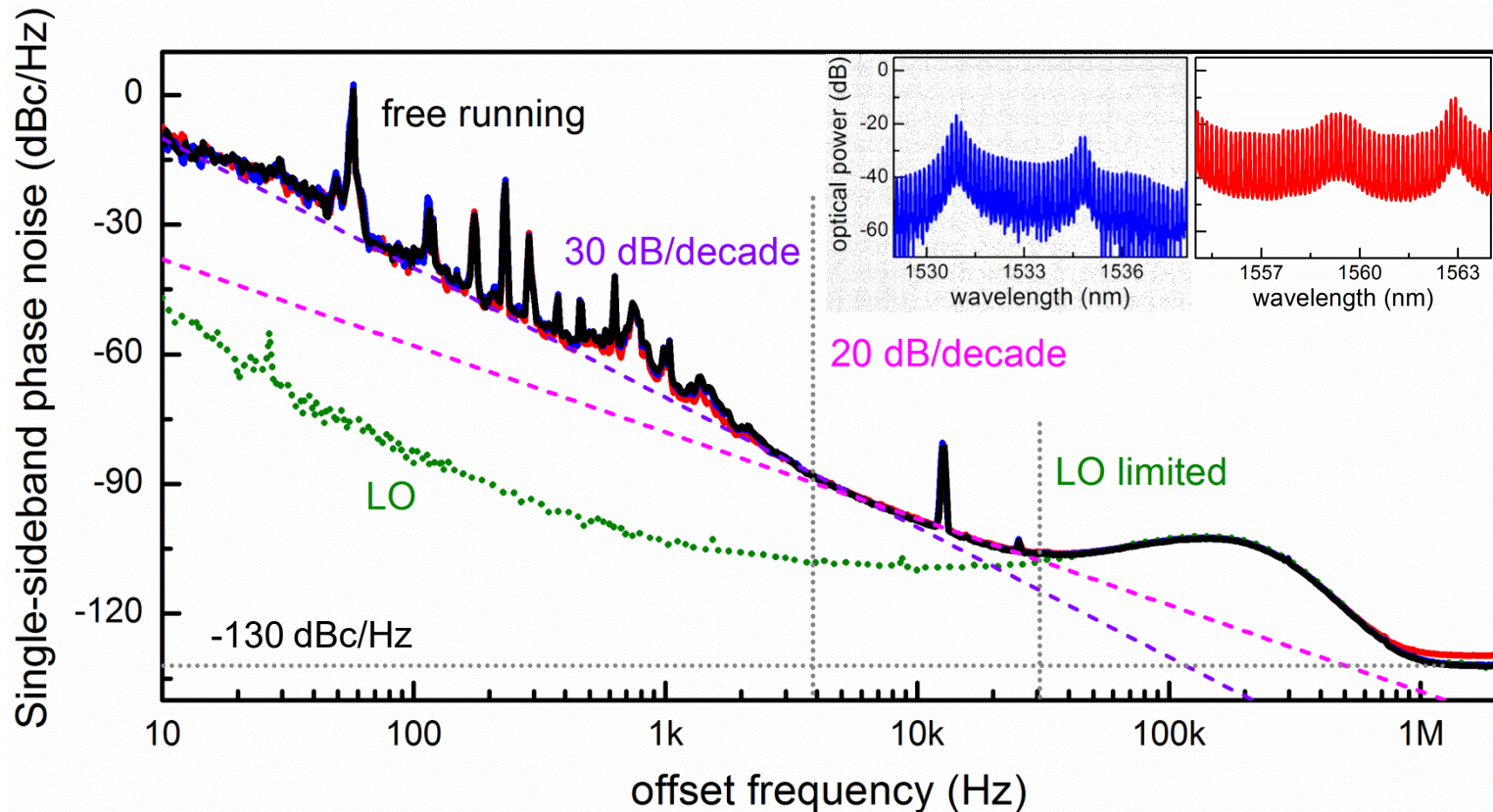


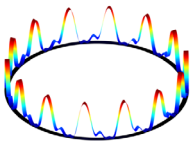


Phase noise analysis of the μ comb oscillator

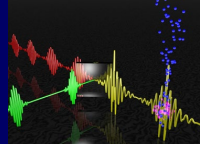


Quantum-noise-limited phase noise has a roll-off of 20 dB/decade and approaches -148 dBc/Hz at 1 MHz offset from the carrier of 17.9 GHz.

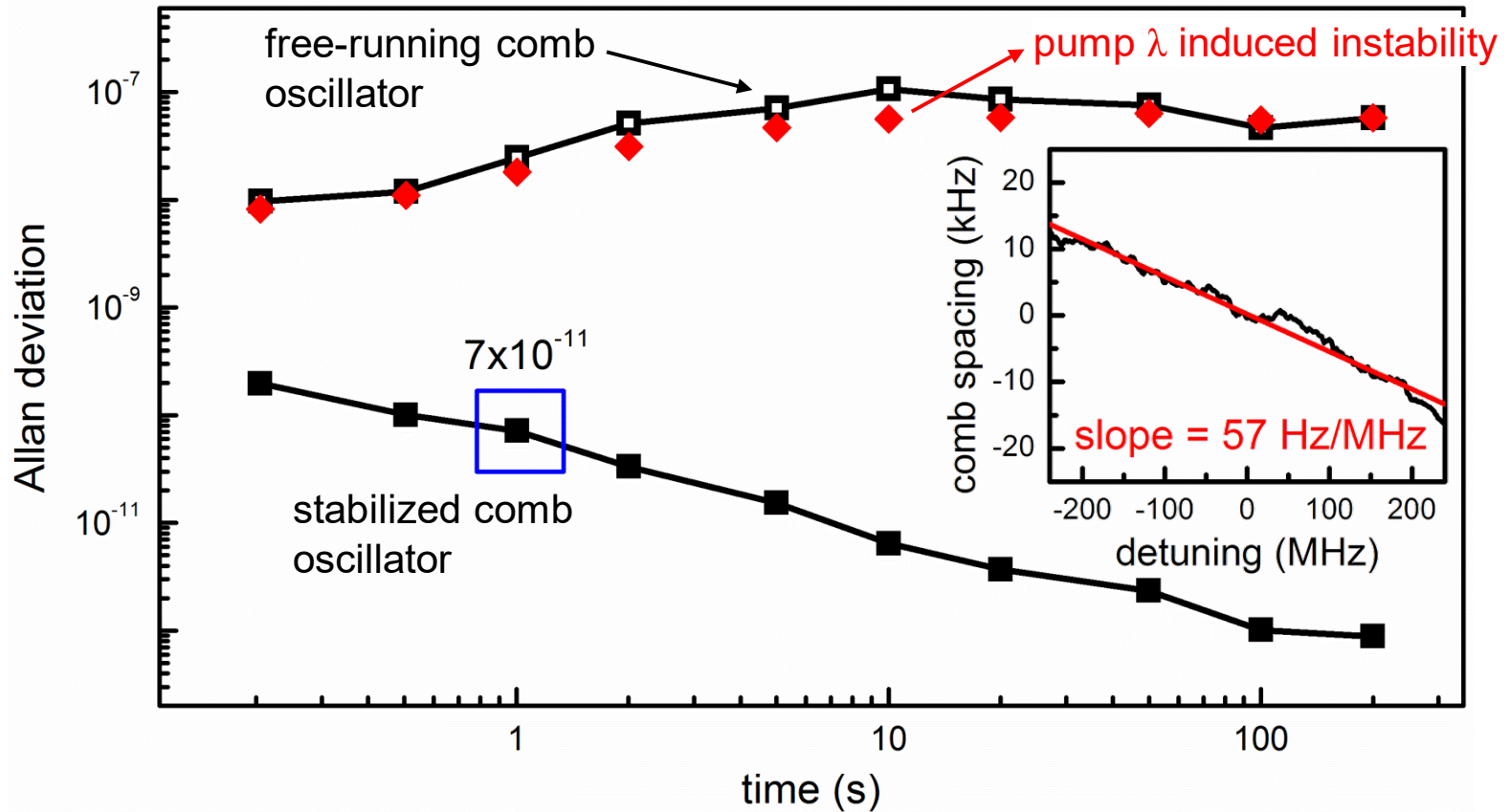


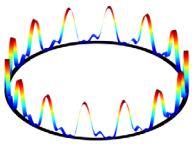


Stability of the μ comb oscillator

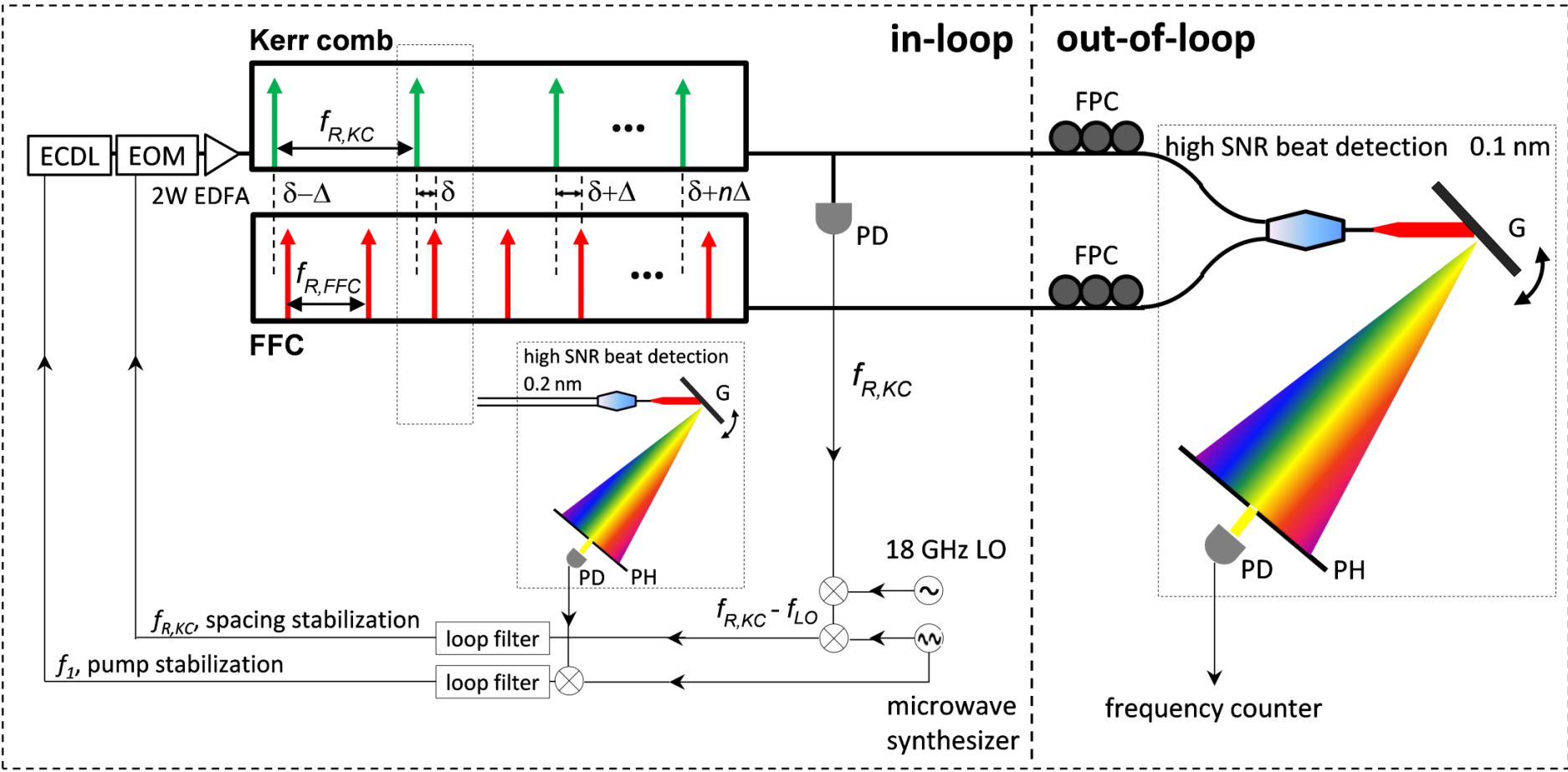
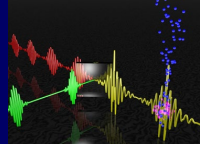


- Pump frequency drift limits the μ comb oscillator's long term frequency stability.
- Allan deviation is improved to 7×10^{-11} at 1 s by a computer-aided pump frequency feedback control.



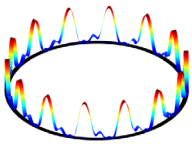


III. High bandwidth comb stabilization

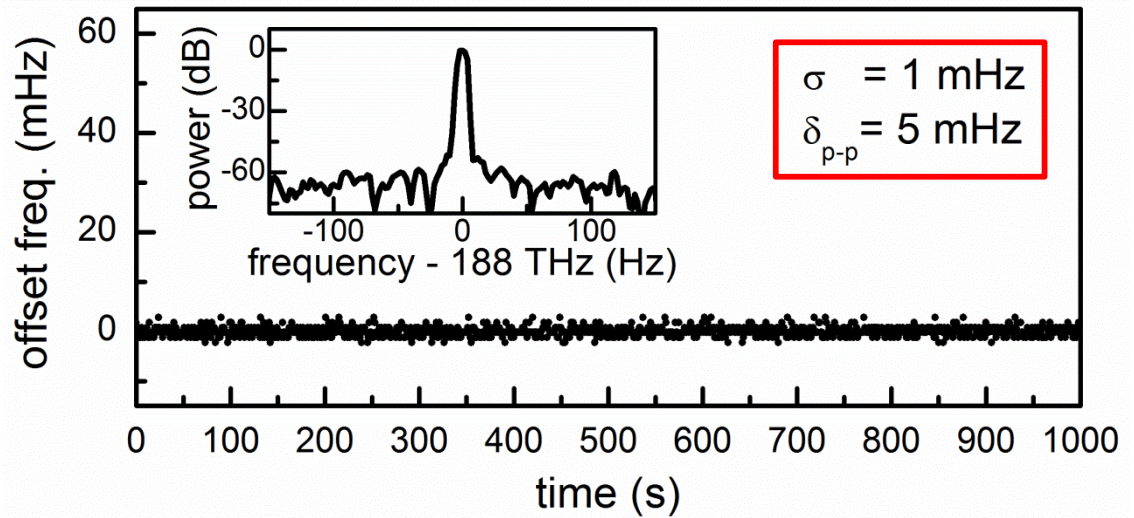
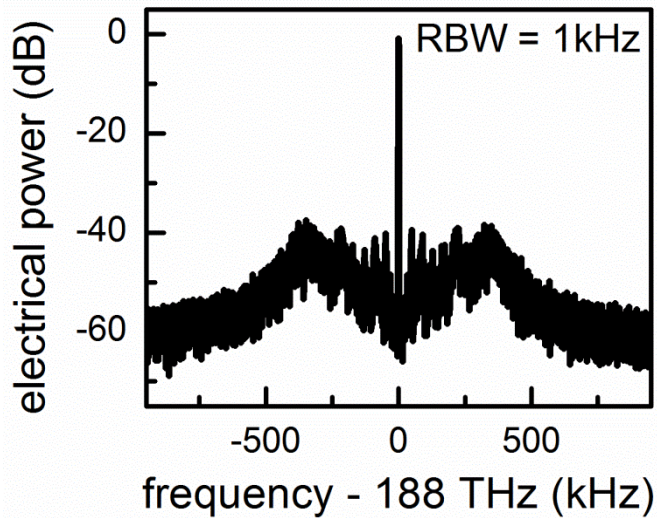
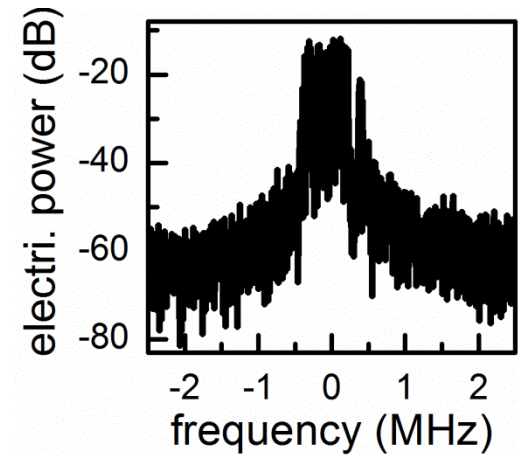
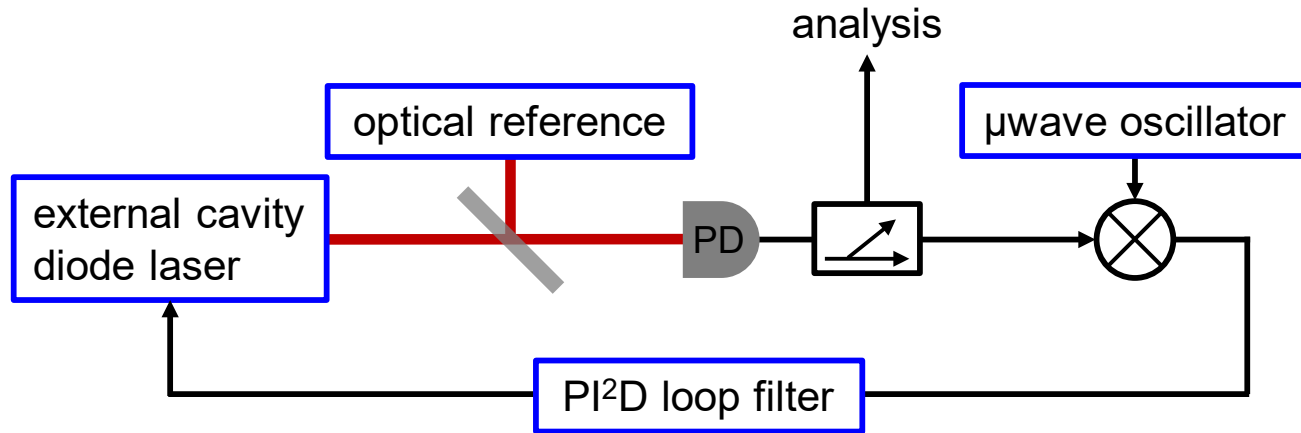
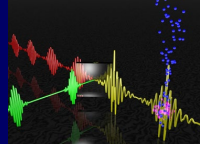


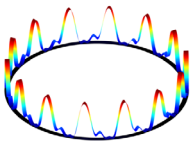
3. High bandwidth comb stabilization achieving a fractional uncertainty of 2.7×10^{-16}
 - Huang *et al.*, *Sci. Adv.* **2**, e1501489 (2016).



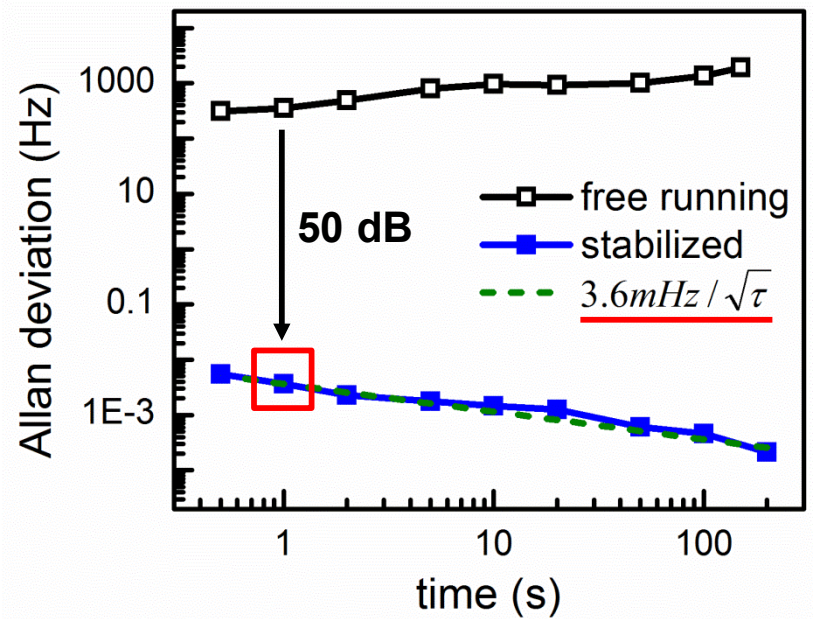
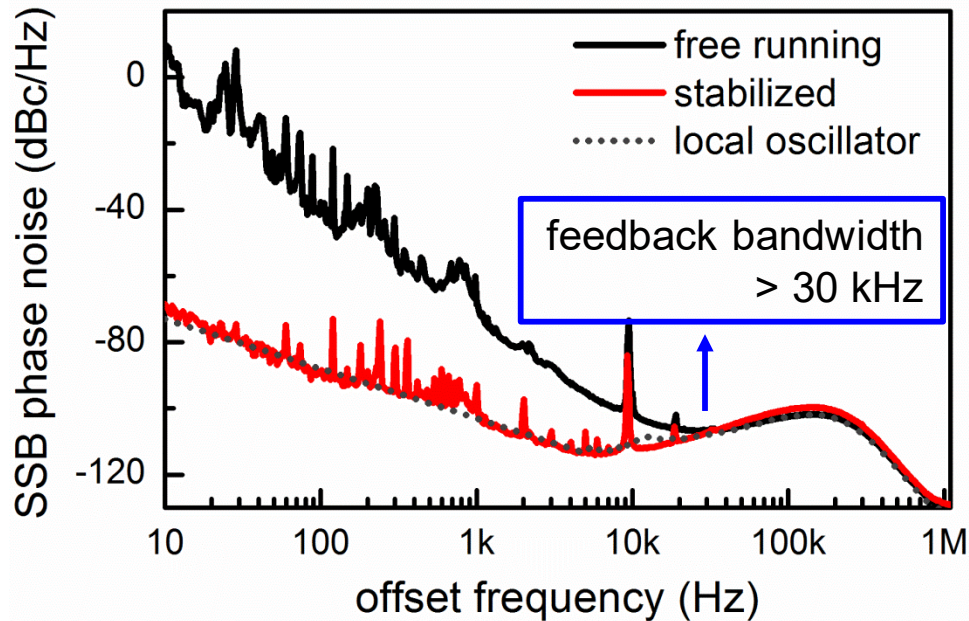
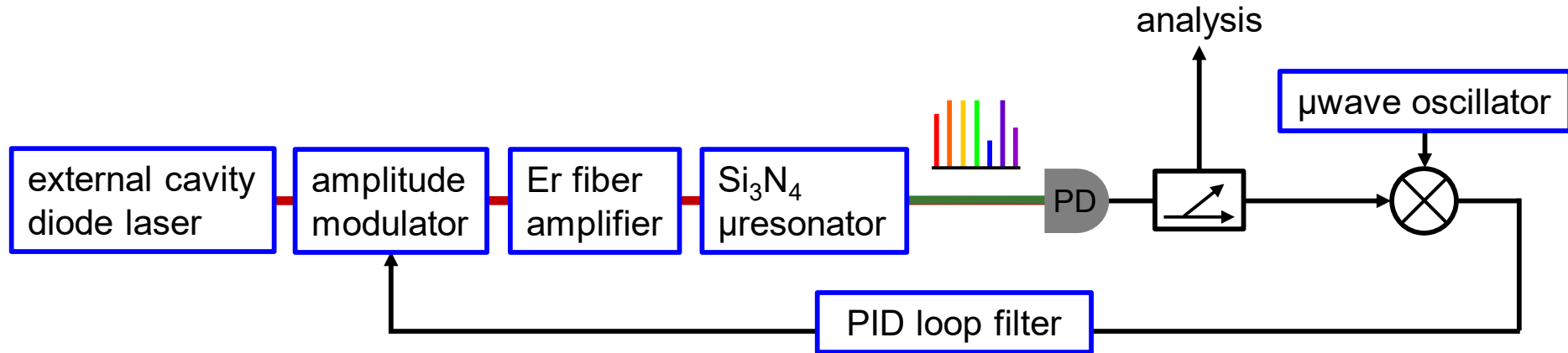
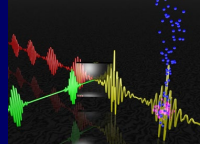


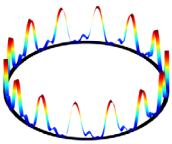
Stabilization of f_{opt} via diode current control



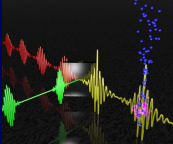


Stabilization of f_{rep} via pump power control

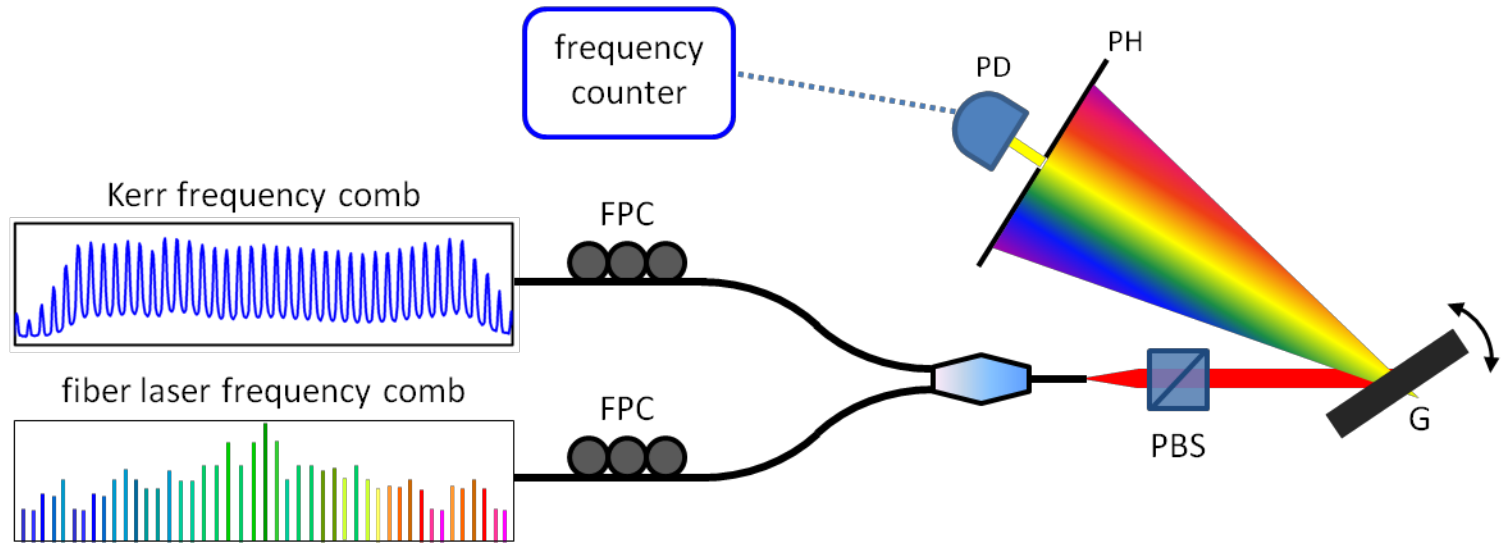
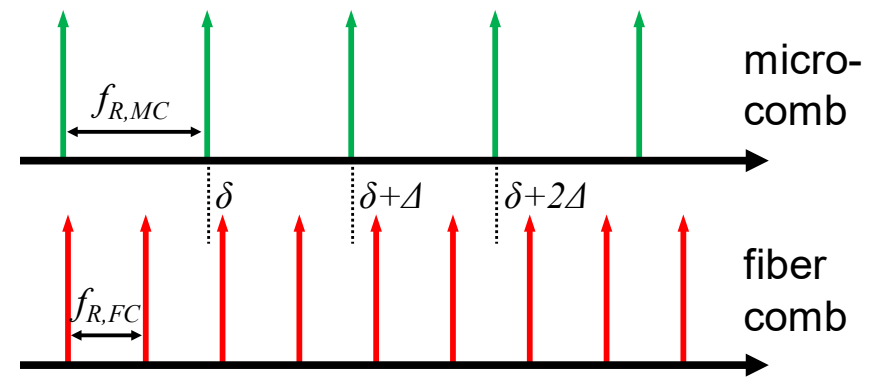


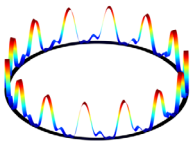


Assessment of the comb frequency uncertainty

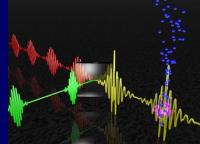


Frequencies of microcomb lines are determined by comparing each line against the state-of-the-art fiber laser frequency comb

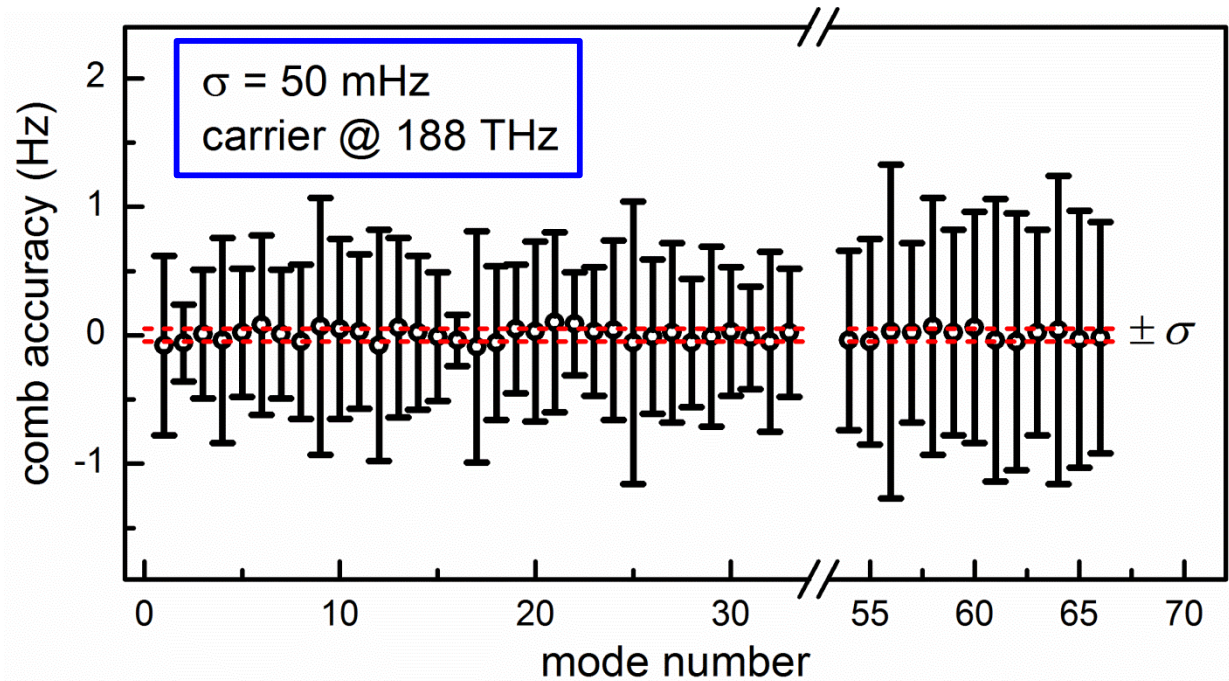
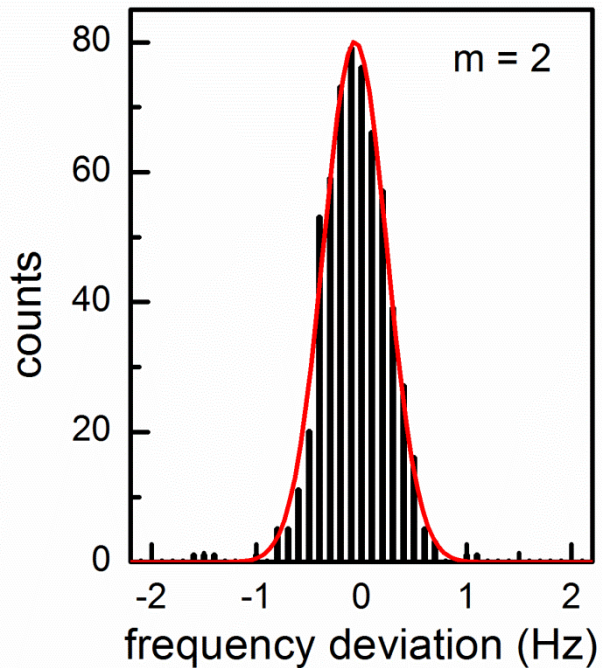


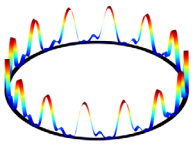


Fractional uncertainty of 2.7×10^{-16}

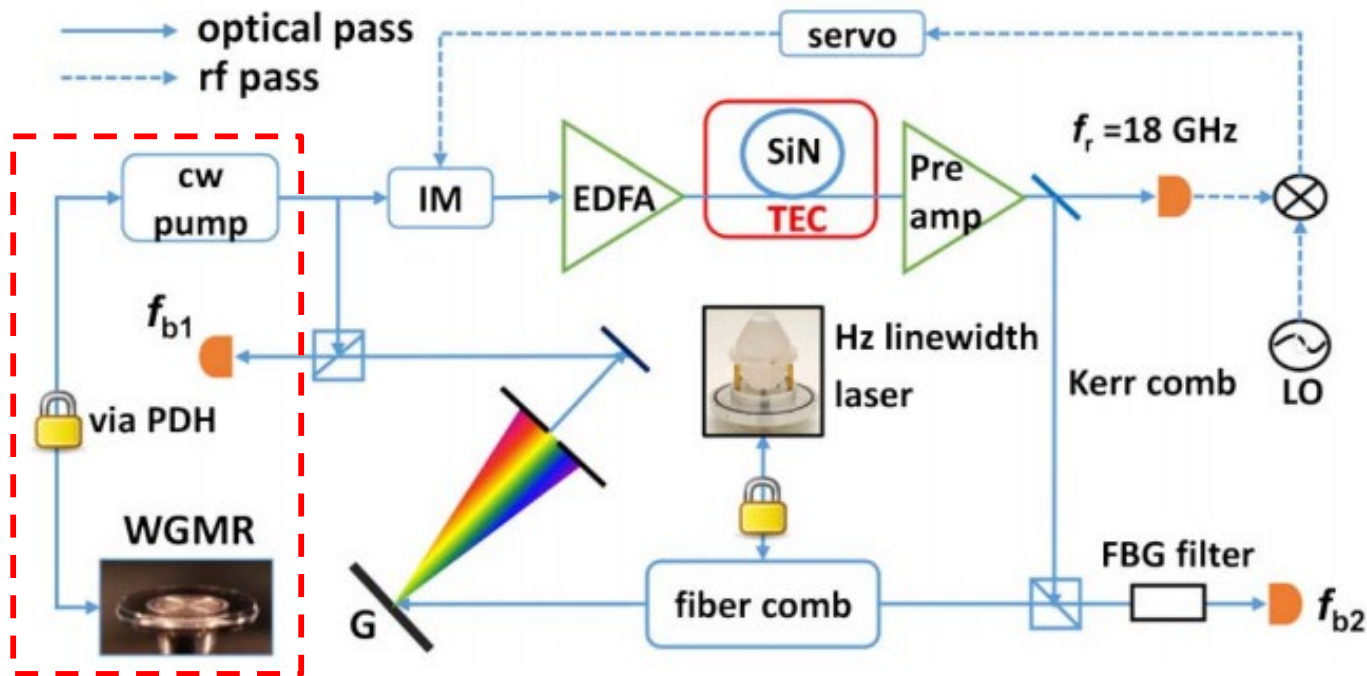
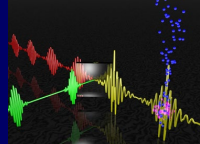


Clockwork using the chip-scale frequency comb as the optical-to-microwave gear can reach a fractional uncertainty of 2.7×10^{-16} .



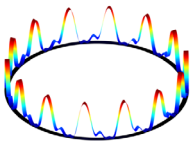


IV. Microresonator stabilized diode laser

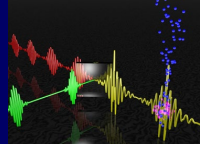


3. High bandwidth comb stabilization achieving a fractional uncertainty of 2.7×10^{-16}
- Huang *et al.*, *Sci. Adv.* **2**, e1501489 (2016).
4. Microresonator stabilized diode laser at the thermodynamical limit of 1.7×10^{-13}
- Lim *et al.*, *Opt. Lett.* **41**, 3706 (2016).

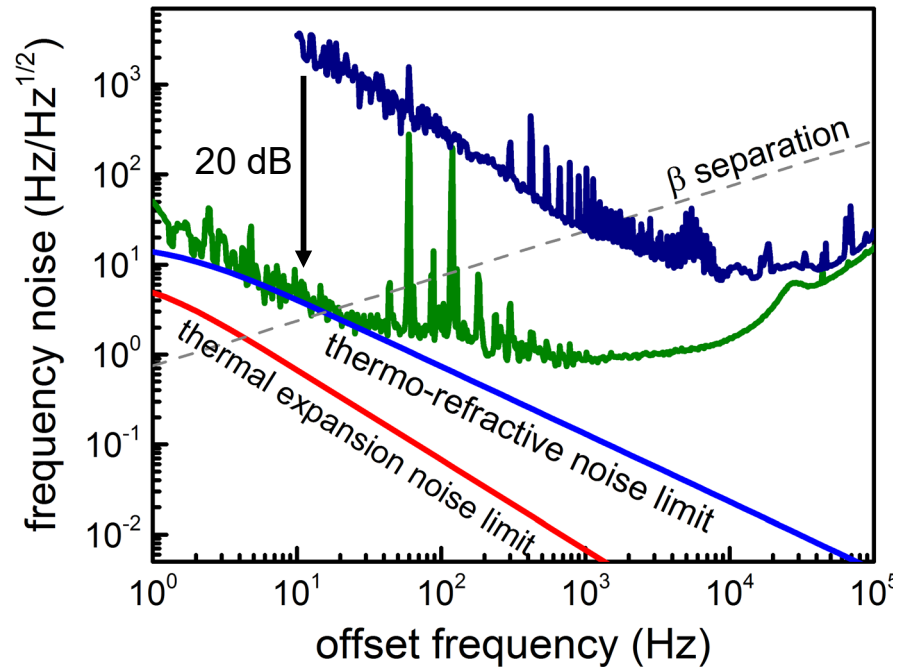
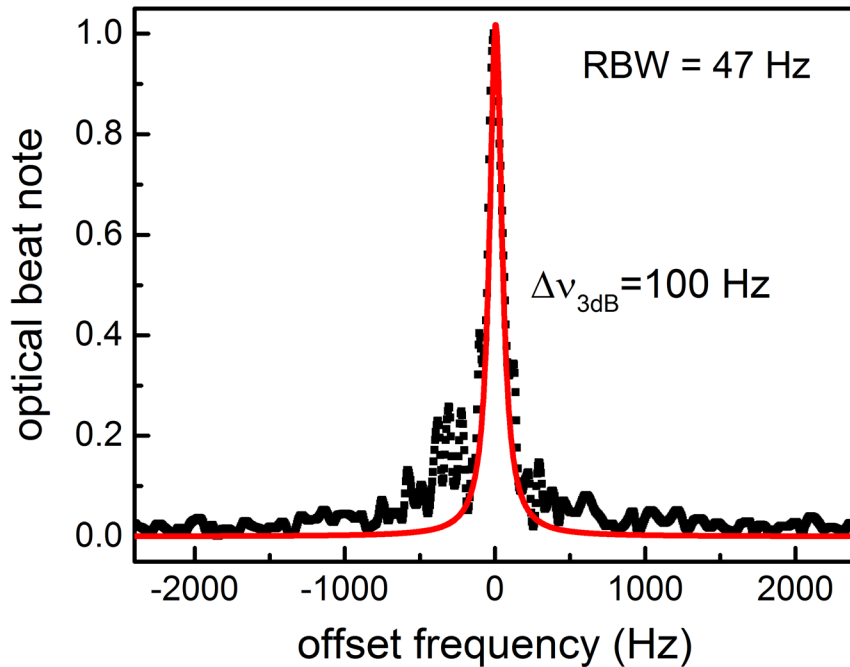


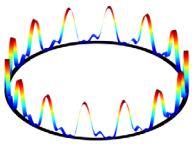


Stabilized laser linewidth and frequency noise

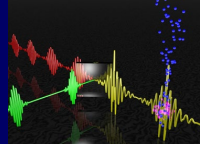


- The stabilized laser linewidth is measured at 100 Hz (25 Hz if the power-line noise is numerically removed).
- The pink frequency noise is a direct consequence of the presence of multiple normal modes of the heat transfer equation in the MgF_2 microresonator.

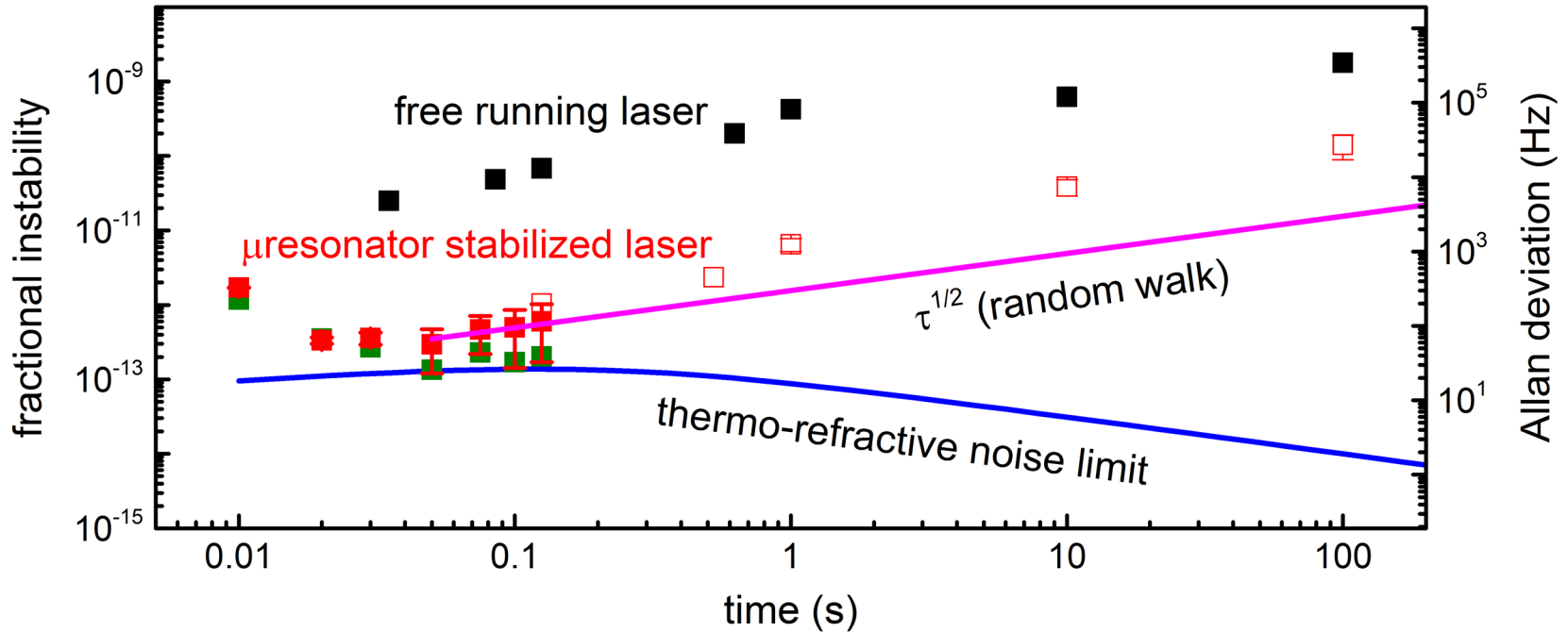


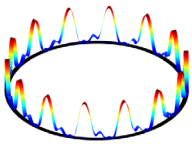


Assessment of the laser frequency instability

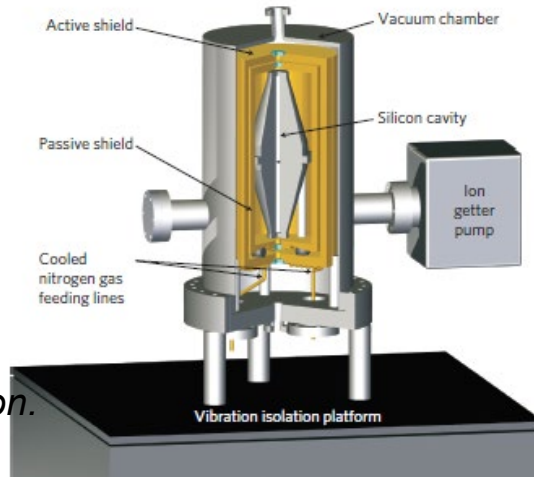
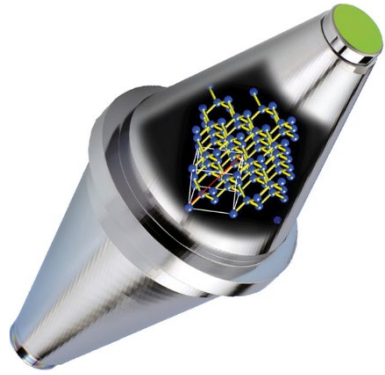
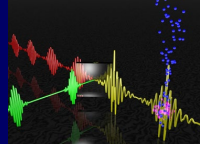


- Fractional instability of the stabilized laser frequency reaches the thermo-refractive noise limit of 1.7×10^{-13} at 100 ms.
- Long-term stability deviates from the random walk noise ($\tau^{1/2}$) due to the digitization error of the used thermo-electric cooler.



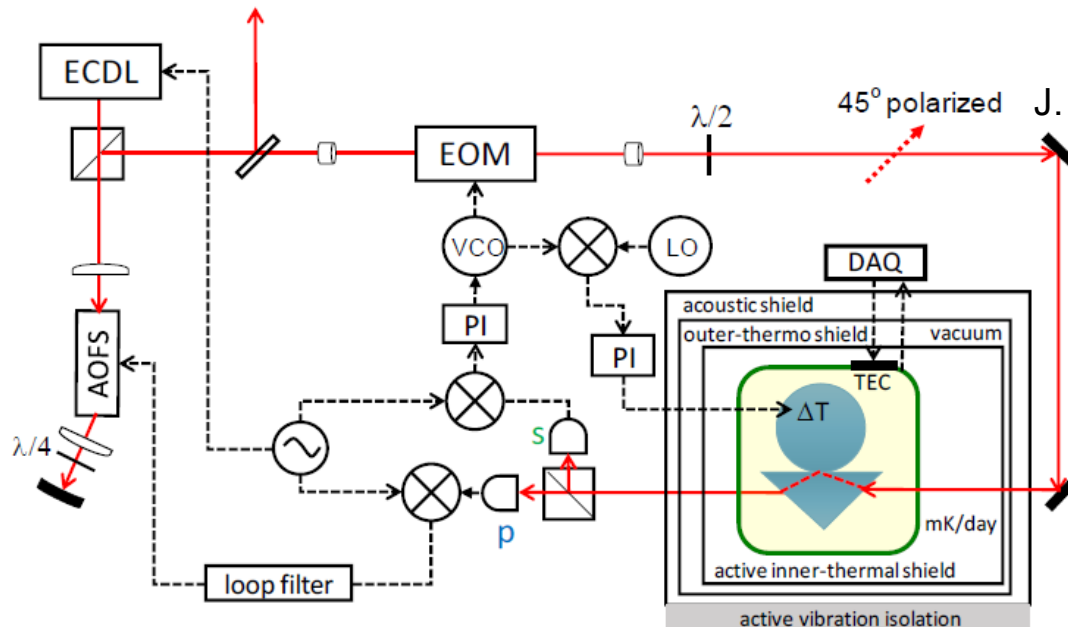


Dual-mode temperature compensation

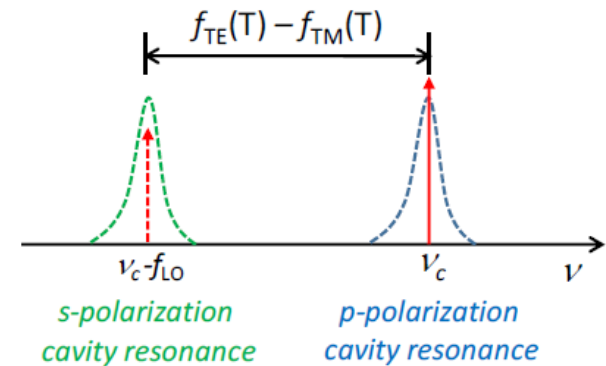


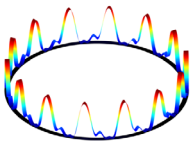
Going from bulk to chip-scale solution, thermal noise induced resonance shift becomes the dominant noise source and active suppression to sub- μK is necessary.

T. Kessler *et al.*, *Nat. Photon.* **6**, 687 (2012).

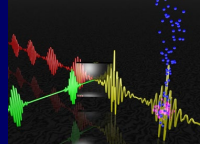


J. Alnis *et al.*, *Phys. Rev. A* **84**, 011804 (2011).

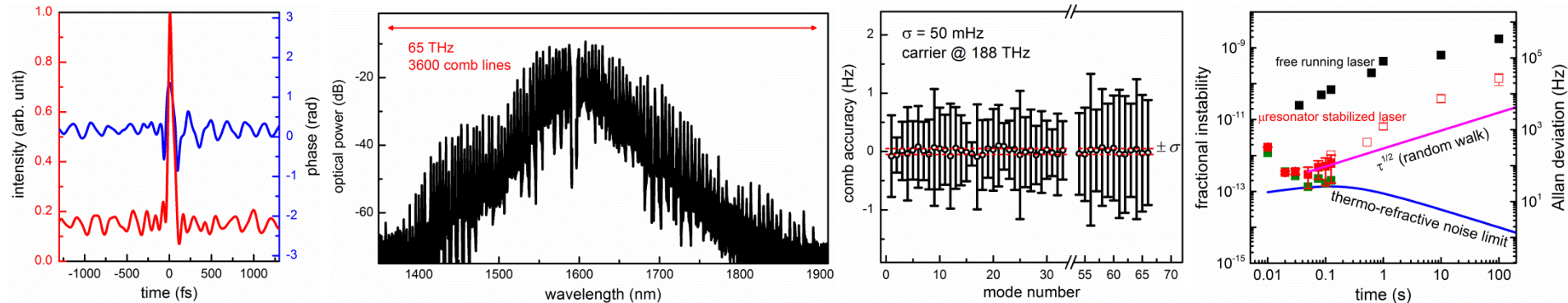


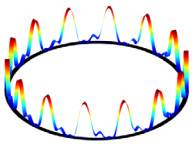


Summary

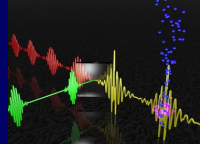


1. Microresonator-based ultrafast light source delivering 74 femtosecond pulse train
- Huang *et al.*, *Phys. Rev. Lett.* **114**, 053901 (2015).
2. Low noise broadband microcomb containing 3,600 coherent frequency teeth
- Huang *et al.*, *Sci. Rep.* **5**, 13355 (2015).
3. High bandwidth comb stabilization achieving a fractional uncertainty of 2.7×10^{-16}
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4. Microresonator stabilized diode laser at the thermodynamical limit of 1.7×10^{-13}
- Lim *et al.*, *Opt. Lett.* **41**, 3706 (2016).





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